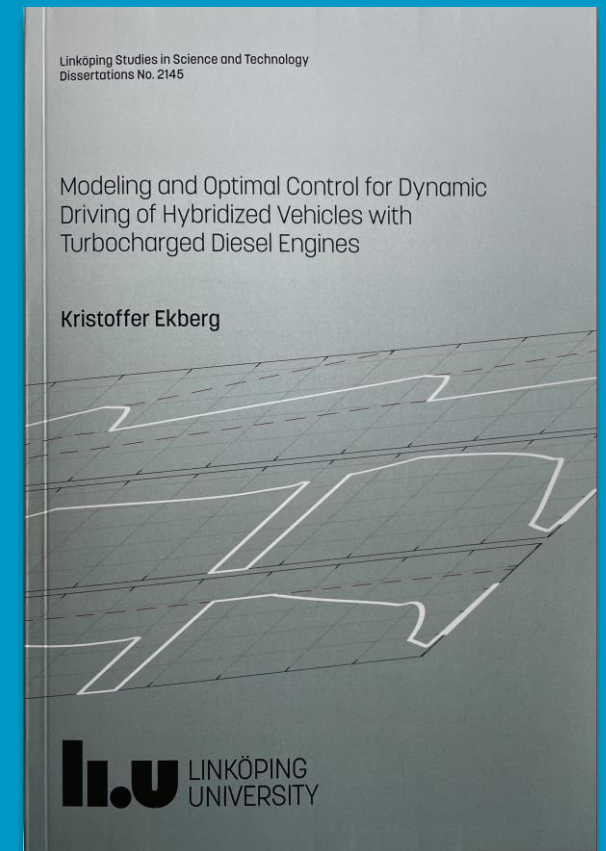


# Modeling and Optimal Control for Dynamic Driving of Hybridized Vehicles with Turbocharged Diesel Engines

Kristoffer Ekberg  
Vehicular Systems  
Department of Electrical Engineering



# Introduction

- Majority of road freight transported by trucks <sup>1</sup>
- Diesel powered 98% <sup>1</sup>
- Diesel emissions <sup>2</sup>:
  - Hydro carbons
  - Particulate emissions (soot)
  - Carbon monoxide
  - Nitrogen oxides and dioxides (NO<sub>x</sub>).



A better fuel economy of produced vehicles will reduce the amount of needed fuel, and consequently the release of  $CO_2$ .

# Trends

- Electrification of powertrains

Results in:

- Increase in system complexity
- More difficult engineering problem, choice of technology and its controls

Inserting electric machines in the powertrain:

- Electric crank shaft motor
- Electric turbocharger

# Thesis Aim

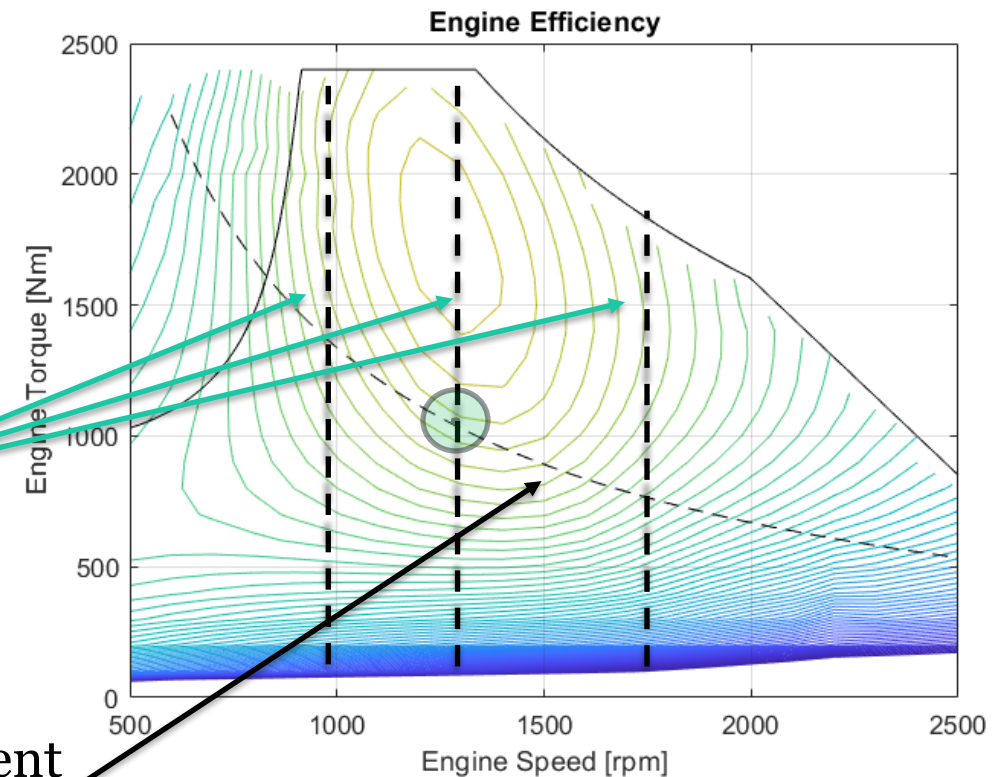
- Reduce the energy needed for accelerating and driving commercial vehicles.
- Methods that solve these problems.
- Knowledge about the relative importance of electric turbocharging and hybrid propulsion technologies on the system performance.

# Propulsion - Achieving improvements

- Diesel engine control
- Load point dependent engine efficiency
- Gear selection for fuel economy

Engine speed due to  
selected gear

Power requirement



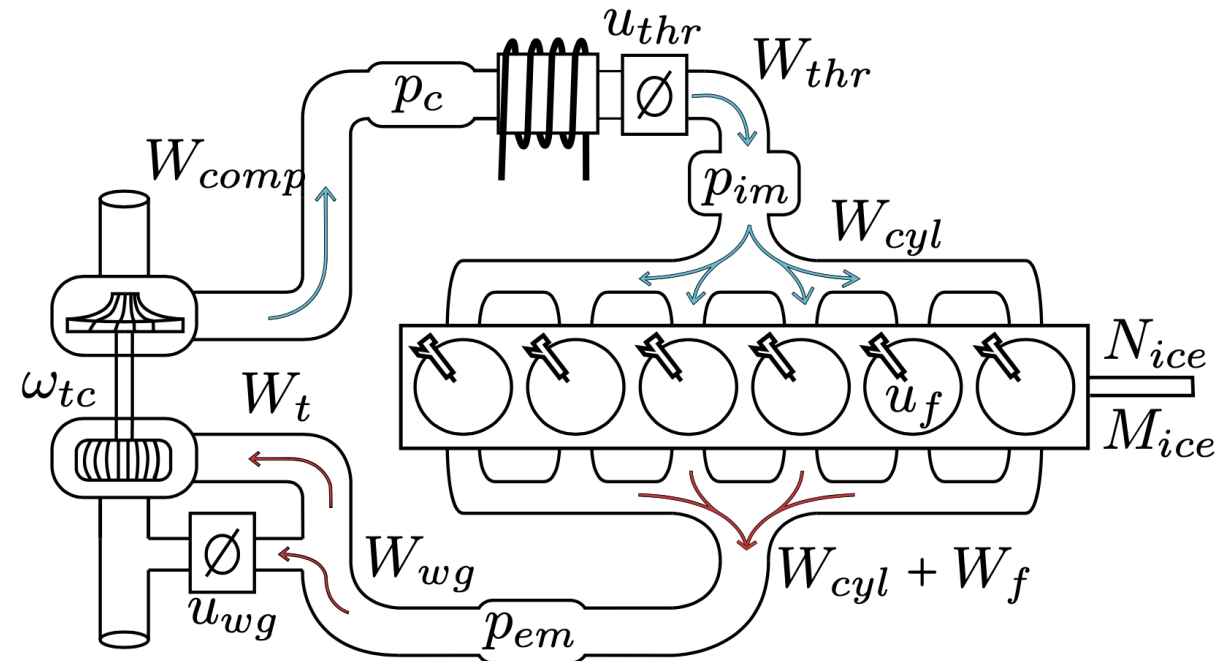
# Turbocharged Compression Ignited (CI) Engine

- Air Fuel Ratio

$$\lambda = \frac{W_{cyl}}{AF_S W_f}$$

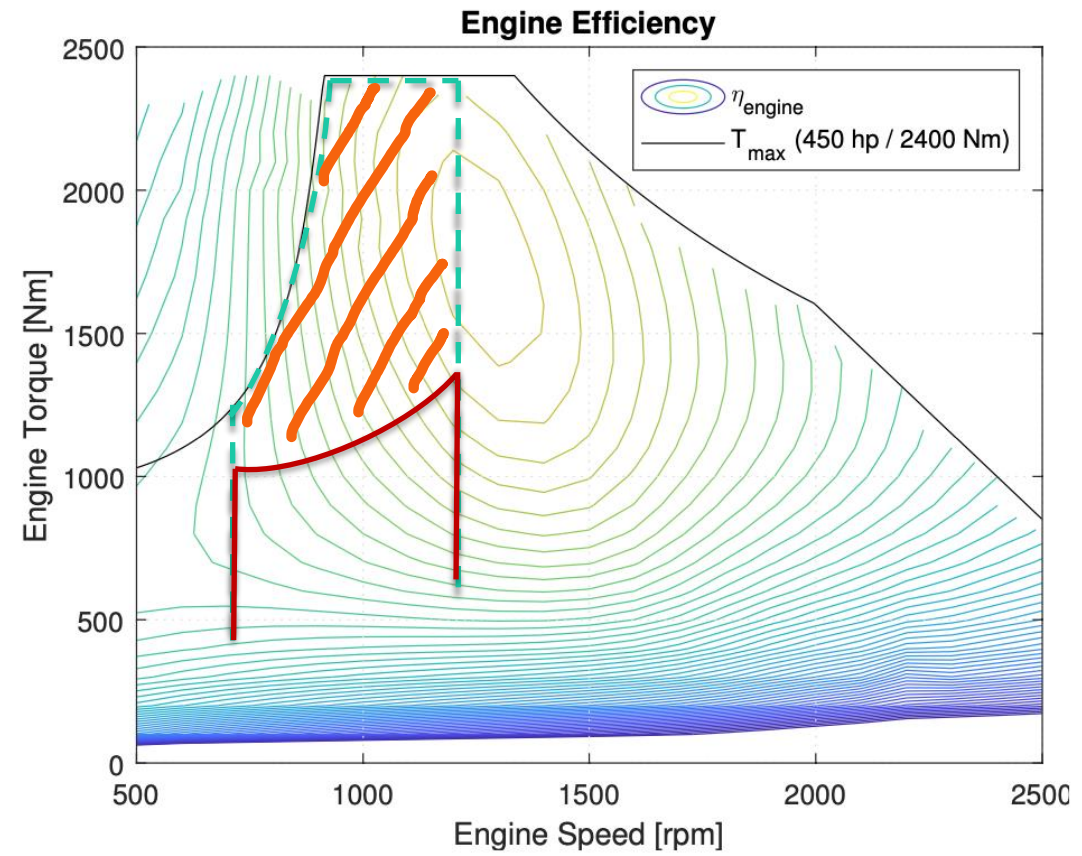
- Restricted due to smoke formation

$$\lambda_{min} < \lambda$$



# Turbocharger Lag

- Transient response
- Risk of black smoke<sup>1</sup>



# Paper I



## Improving Fuel Economy and Acceleration by Electric Turbocharger Control for Heavy Duty Long Haulage<sup>1</sup>

Kristoffer Ekberg and Lars Eriksson

Department of Electrical Engineering

Division of Vehicular Systems

SE-581 83 Linköping, Sweden

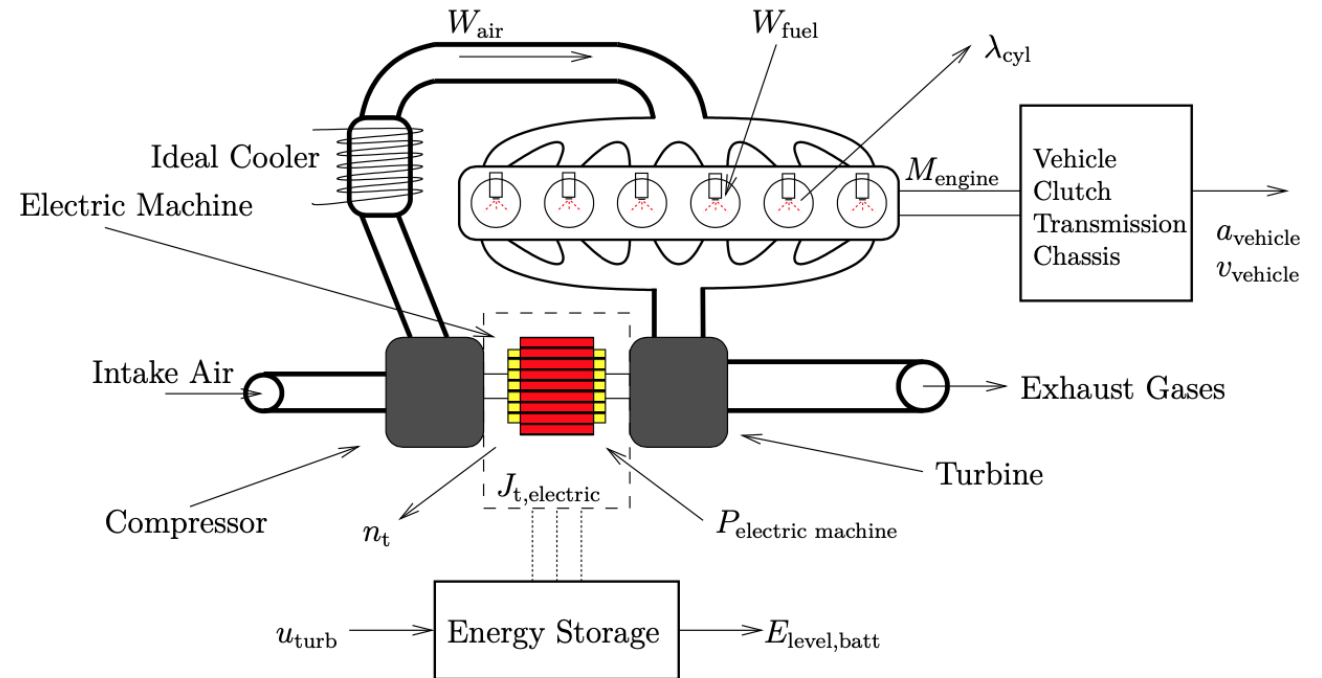
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<sup>1</sup>Reprinted, with permission, from Kristoffer Ekberg and Lars Eriksson (2017). "Improving Fuel Economy and Acceleration by Electric Turbocharger Control for Heavy Duty Long Haulage." In: *IFAC-PapersOnLine* 50.1. 20th IFAC World Congress, pp. 11052–11057. ISSN: 2405-8963. DOI: <https://doi.org/10.1016/j.ifacol.2017.08.2486>. The formatting is restricted to adjusting the appearance of the text, figures, tables, and the reference style without changing their content.



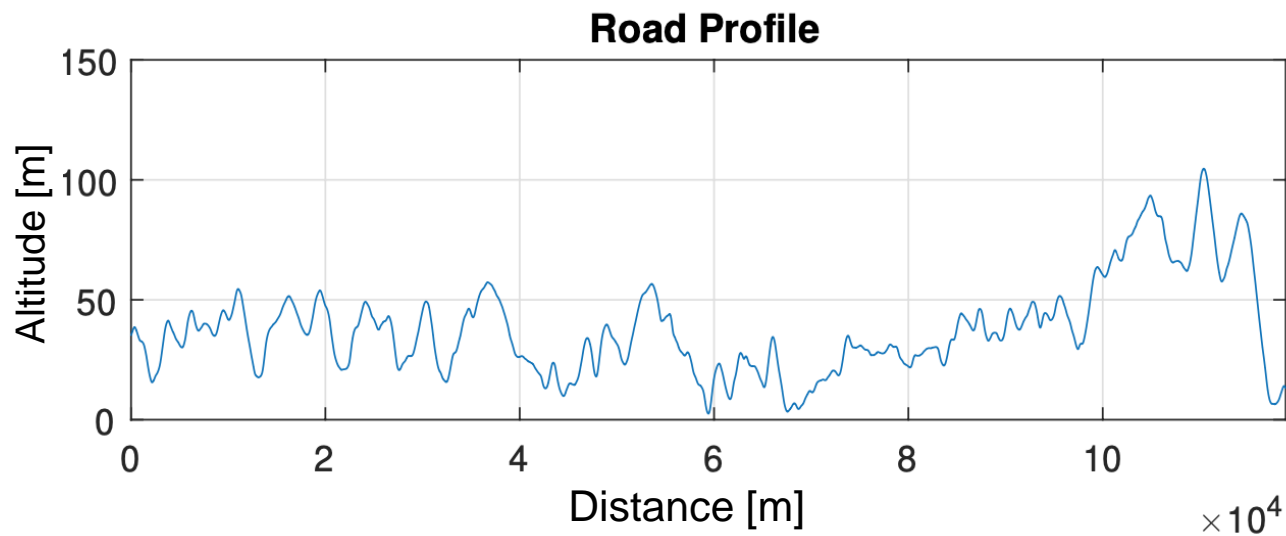
# Electric Topologies for Boost Control

- Extra power input
- Regeneration



# Paper I – Results – Long Haulage Driving

- With electric turbocharger: 37.48 l/100km
- Without electric turbocharger: 37.82 l/100km
- 0.9% fuel saving for the undulated driving mission



# Optimal Control

- Mathematical way to find system controls to minimize a defined cost
- Different methods
  - Dynamic Programming
  - Numerical method - Direct collocation
- Model requirements

# Paper II



## Optimal Control of Wastegate Throttle and Fuel Injection for a Heavy-Duty Turbocharged Diesel Engine During Tip-In<sup>1</sup>

Kristoffer Ekberg, Viktor Leek, and Lars Eriksson

Department of Electrical Engineering  
Division of Vehicular Systems  
SE-581 83 Linköping, Sweden

<sup>1</sup>Reprinted, with permission, from Kristoffer Ekberg, Viktor Leek, and Lars Eriksson (2019). "Optimal Control of Wastegate Throttle and Fuel Injection for a Heavy-Duty Turbocharged Diesel Engine During Tip-In." In: *SIMS 2017, Reykjavik, Island*. DOI: <http://dx.doi.org/10.3384/ecp17138317>. The formatting is restricted to adjusting the appearance of the text, figures, tables, and the reference style without changing their content.

## Paper II – Optimal Control

- Find a stationary point at a defined engine speed and delivered torque, which is fuel optimal.
- Find the least time consuming control to perform a Tip-In, from the stationary point, to a point where the requested torque is available.

$$\min_{x(t), u(t)} t_f, \quad \text{s. t.}$$

$$\begin{aligned} \dot{x}(t) &= f(x(t), u(t)) \\ x_{min} &\leq x(t) \leq x_{max} \\ u_{min} &\leq u(t) \leq u_{max} \\ 0 &\leq \phi(t) \leq 1/\lambda_{min} \\ BSR_{min} &\leq BSR(t) \leq BSR_{max} \\ \dot{m}_c(t) &\geq \dot{m}_{zsl}(N_t) \\ \dot{m}_c(t) &\leq \dot{m}_{ch}(N_t) \\ N_t(t) &\geq c_{22} \quad (\text{from Equation (11c)}) \\ N_e(t) &= N_{e, fixed} \end{aligned}$$

# Paper II – Constraints

The problem constraints are formulated in the following way

$$\dot{x}(t) = f(x(t), u(t))$$

$$x_{min} \leq x(t) \leq x_{max}$$

$$u_{min} \leq u(t) \leq u_{max}$$

$$0 \leq \phi(t) \leq 1/\lambda_{min}$$

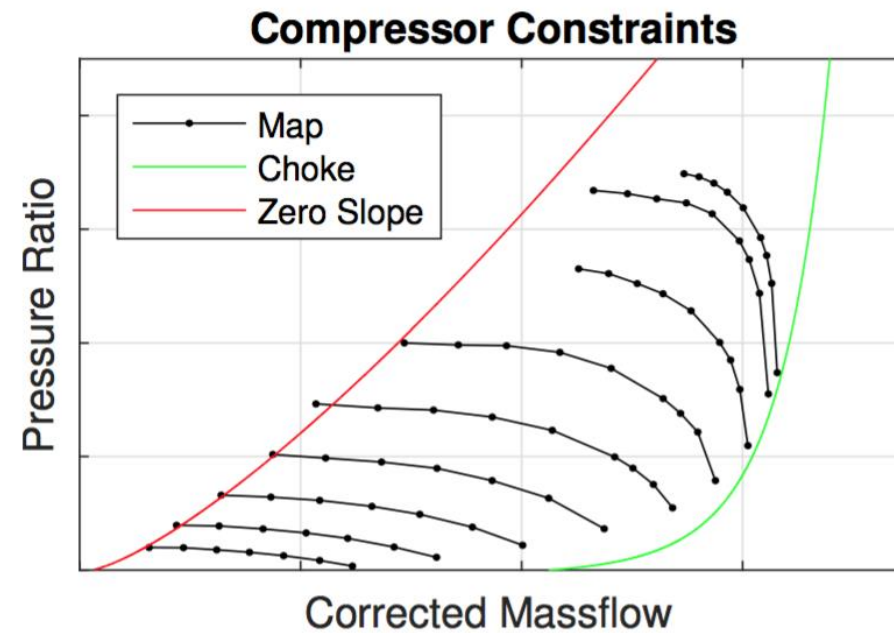
$$BSR_{min} \leq BSR(t) \leq BSR_{max}$$

$$\dot{m}_c(t) \geq \dot{m}_{zsl}(N_t)$$

$$\dot{m}_c(t) \leq \dot{m}_{ch}(N_t)$$

$$N_t(t) \geq c_{22} \text{ (from Equation (11c))}$$

$$N_e(t) = N_{e, fixed}$$



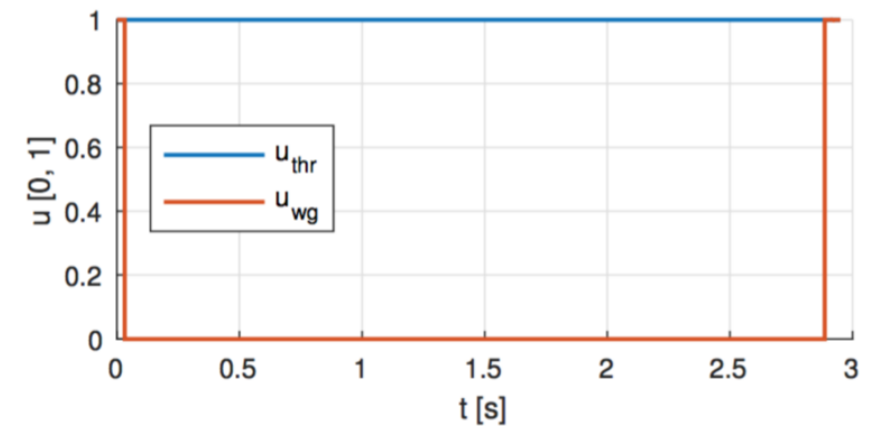
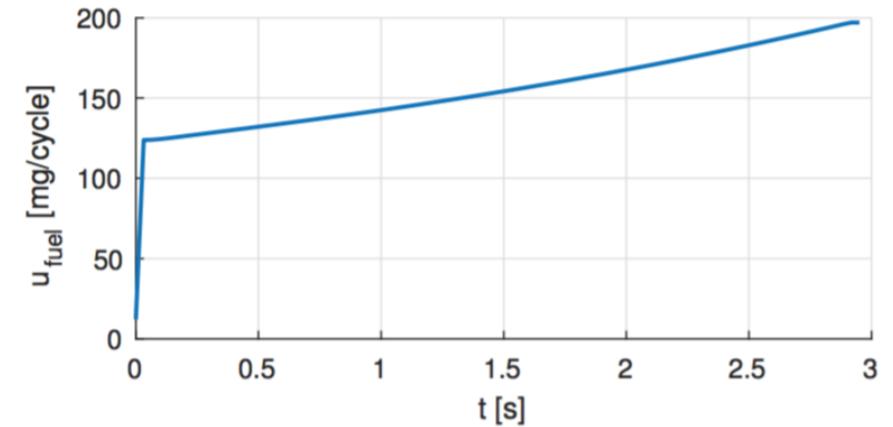
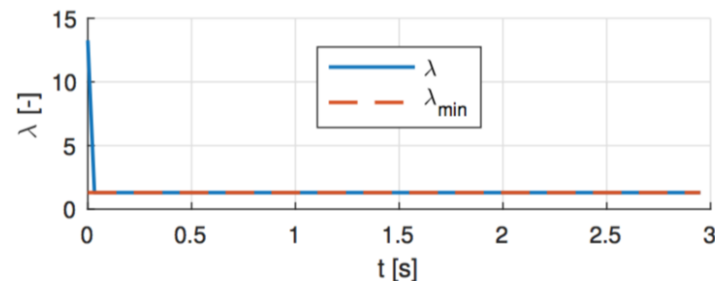
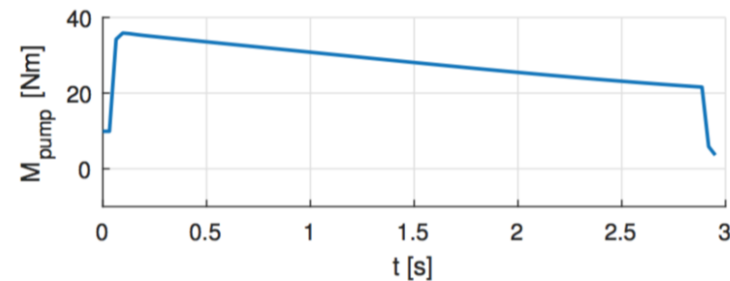
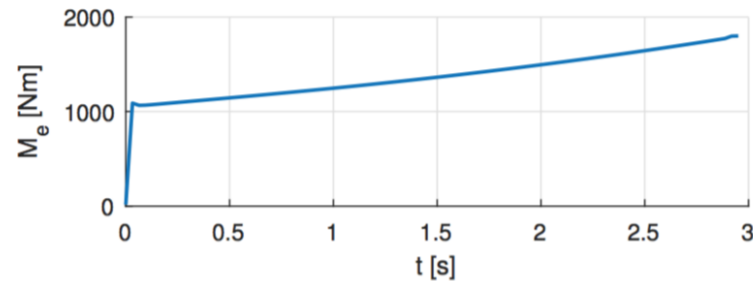
# Paper II – Results – Optimal Control

Time optimal  
Tip-In at fixed  
engine speed

$$x(0) = x_0$$

$$u(0) = u_0$$

$$M_e(t_f) = M_{e,des}$$



# Paper III



## Modeling and Validation of an Open-Source Mean Value Heavy-Duty Diesel Engine Model<sup>1</sup>

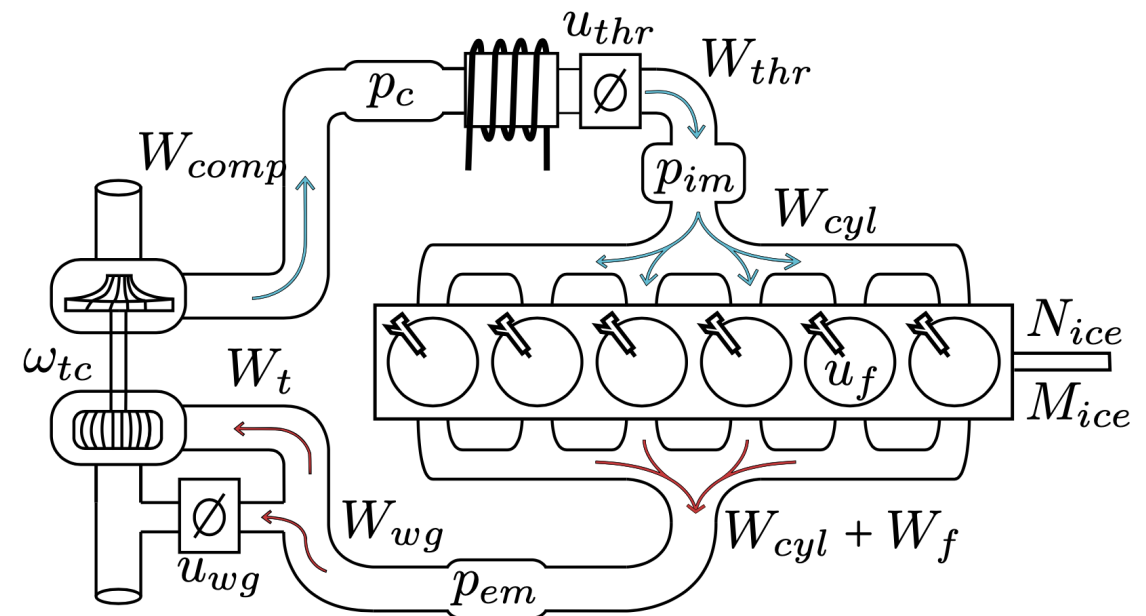
Kristoffer Ekberg, Viktor Leek, and Lars Eriksson  
Department of Electrical Engineering  
Division of Vehicular Systems  
SE-581 83 Linköping, Sweden

<sup>1</sup>Reprinted, with permission, from Kristoffer Ekberg, Viktor Leek, and Lars Eriksson (Dec. 2018). "Modeling and Validation of an Open-Source Mean Value Heavy-Duty Diesel Engine Model." In: *Simulation Notes Europe* 28(4), pp. 197–204. ISSN: 2306-0271. DOI: <https://doi.org/10.11128/sne.28.tn.10451>. The formatting is restricted to adjusting the appearance of the text, figures, tables, and the reference style without changing their content.



## Paper III – Contributions

- Models and validates a model of a 13 liter CI engine and release the model as open source.
- Load dependent engine efficiency.

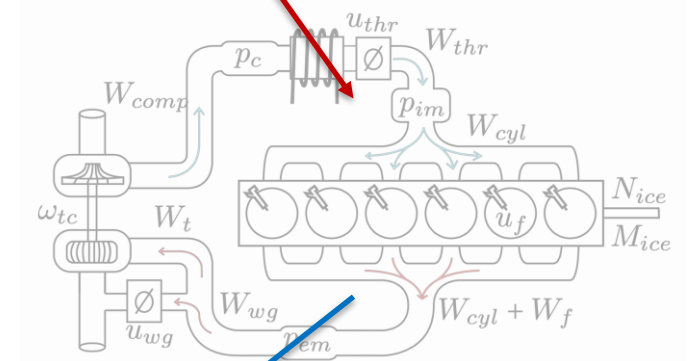


# Paper III – Available Data

## Dataset

- A. Stationary measurement data
- B. GT Power Simulation
- C. Compressor map
- D. Turbine map
- E. Dynamic measurement data
- F. Throttle effective area

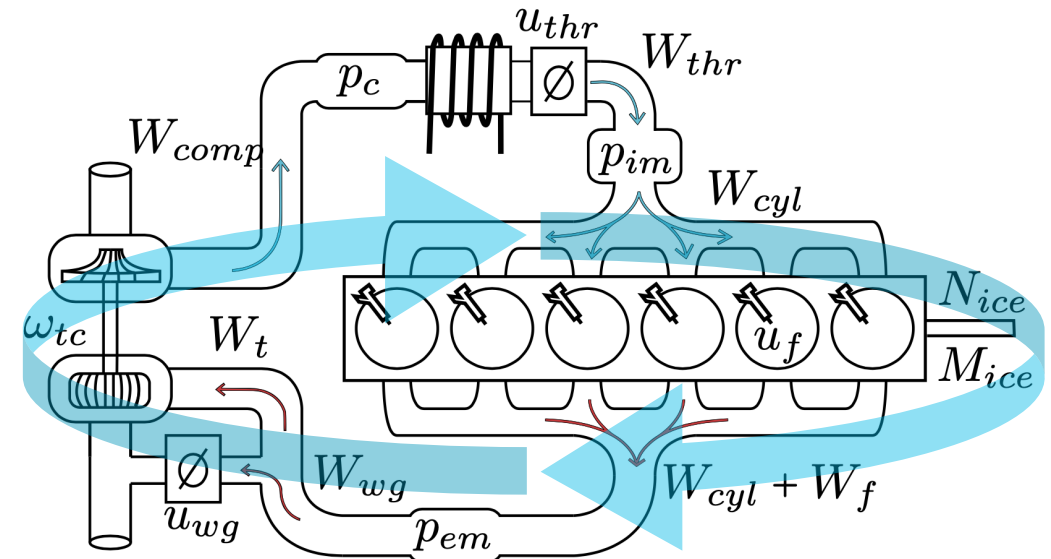
## Parametrization



## Validation

## Paper III – Model Parametrization

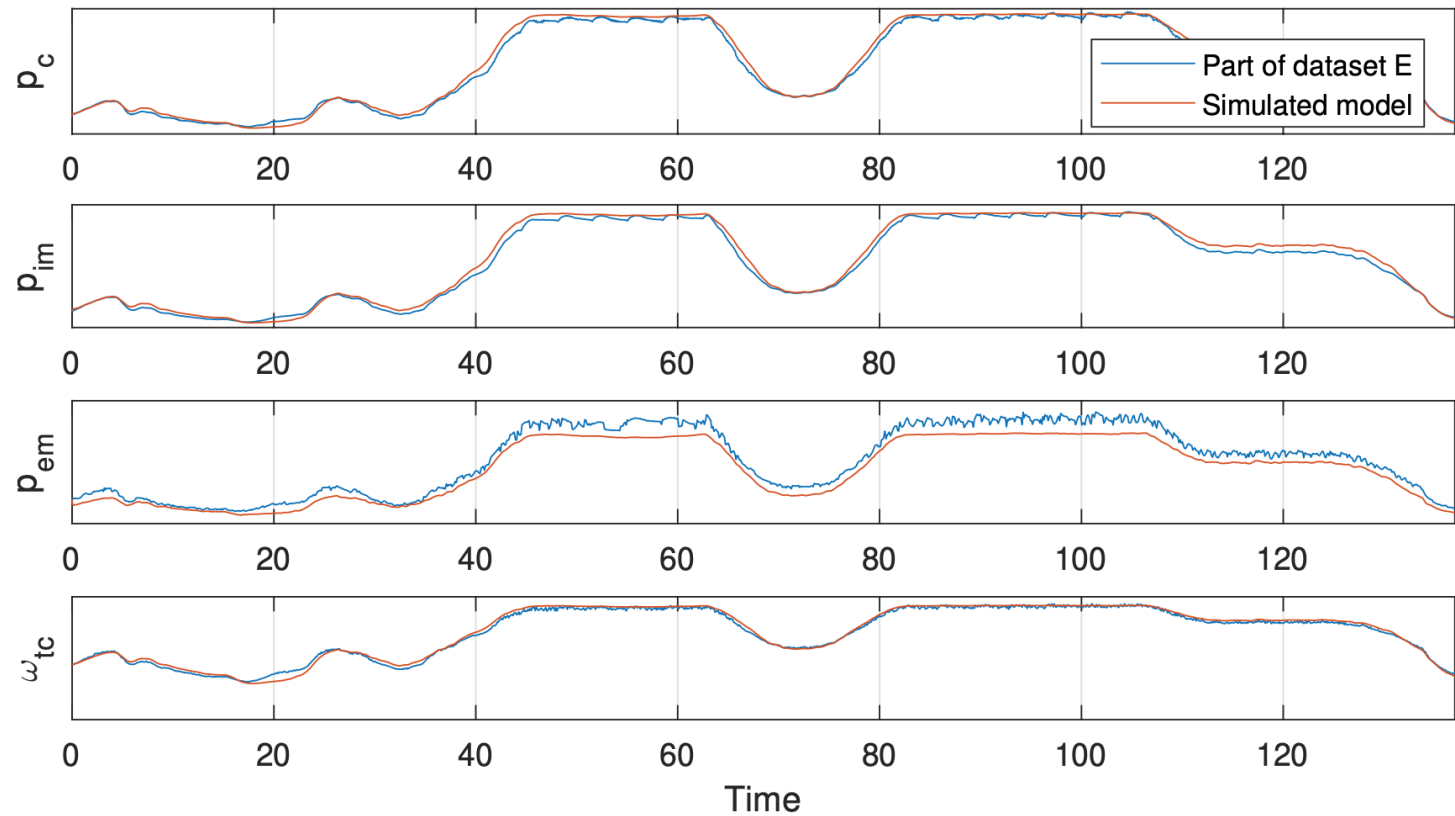
- Closed loop model (stationary)
  - Controlling the wastegate.
  - Individual cost to update sub-model parameters.



$$\theta^* = \arg \min_{\theta} \left( \sum_{k=1}^K e_k^2(\theta) + C \sum_{i=1}^I \left( \mu_i \frac{\theta_i^* - \theta_i}{\theta_i^*} \right)^2 \right)$$

# Paper III – Dynamic Validation

- Stationary and dynamic levels are well represented.



# Paper IV



## Development and Analysis of Optimal Control Strategy for Gear Changing Patterns During Acceleration <sup>1</sup>

**Kristoffer Ekberg and Lars Eriksson**

Department of Electrical Engineering  
Division of Vehicular Systems  
SE-581 83 Linköping, Sweden

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<sup>1</sup>Reprinted, with permission, from Kristoffer Ekberg and Lars Eriksson (2019). "Development and Analysis of Optimal Control Strategy for Gear Changing Patterns During Acceleration." In: *IFAC-PapersOnLine* 52.5. 9th IFAC Symposium on Advances in Automotive Control AAC 2019, pp. 316–321. ISSN: 2405-8963. doi: <https://doi.org/10.1016/j.ifacol.2019.09.051>. The formatting is restricted to adjusting the appearance of the text, figures, tables, and the reference style without changing their content.

## Paper IV – Contribution

Method for solving fuel optimal accelerations, while simultaneously solving for gear shifts and engine dynamics.

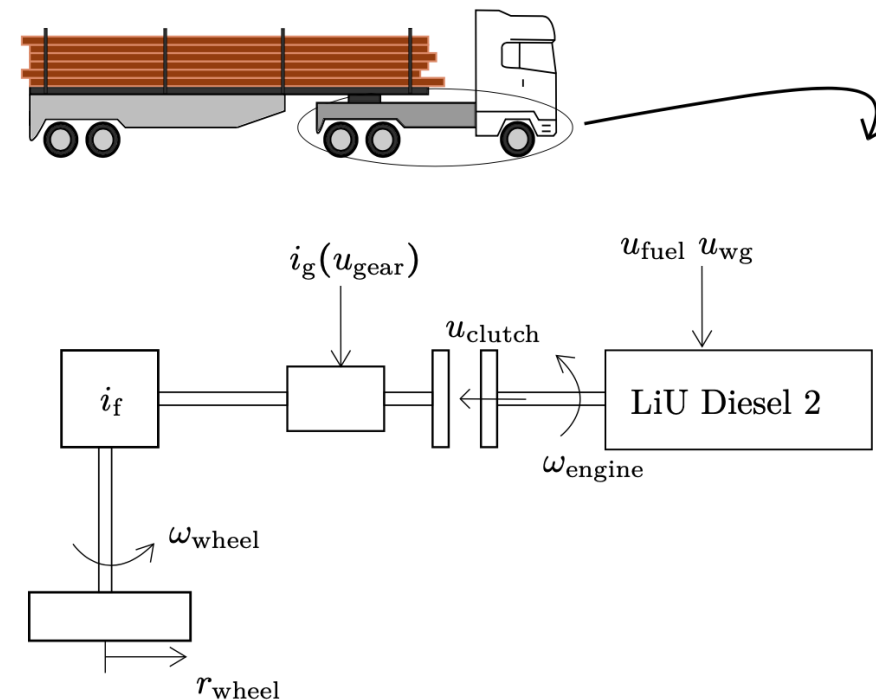
### Scenario:

Accelerate a vehicle from slow rolling speed, to a pre-defined target speed (30 km/h) to the least fuel cost.

# Paper IV – Model

Table 7.1: Model states and control signals.

State	Description
$p_{im}$	Intake manifold pressure
$p_{em}$	Exhaust manifold pressure
$\omega_{tc}$	Turbocharger rotational speed
$\omega_{engine}$	Engine rotational speed
$\omega_{wheel}$	Wheel rotational speed
$X_{distance}$	Driven distance
Control	Description
$u_{fuel}$	Fuel injection
$u_{wg}$	Wastegate position
$u_{clutch}$	Clutch torque
$u_{gear}$	Selected gear



# Paper IV – Results - All Gears

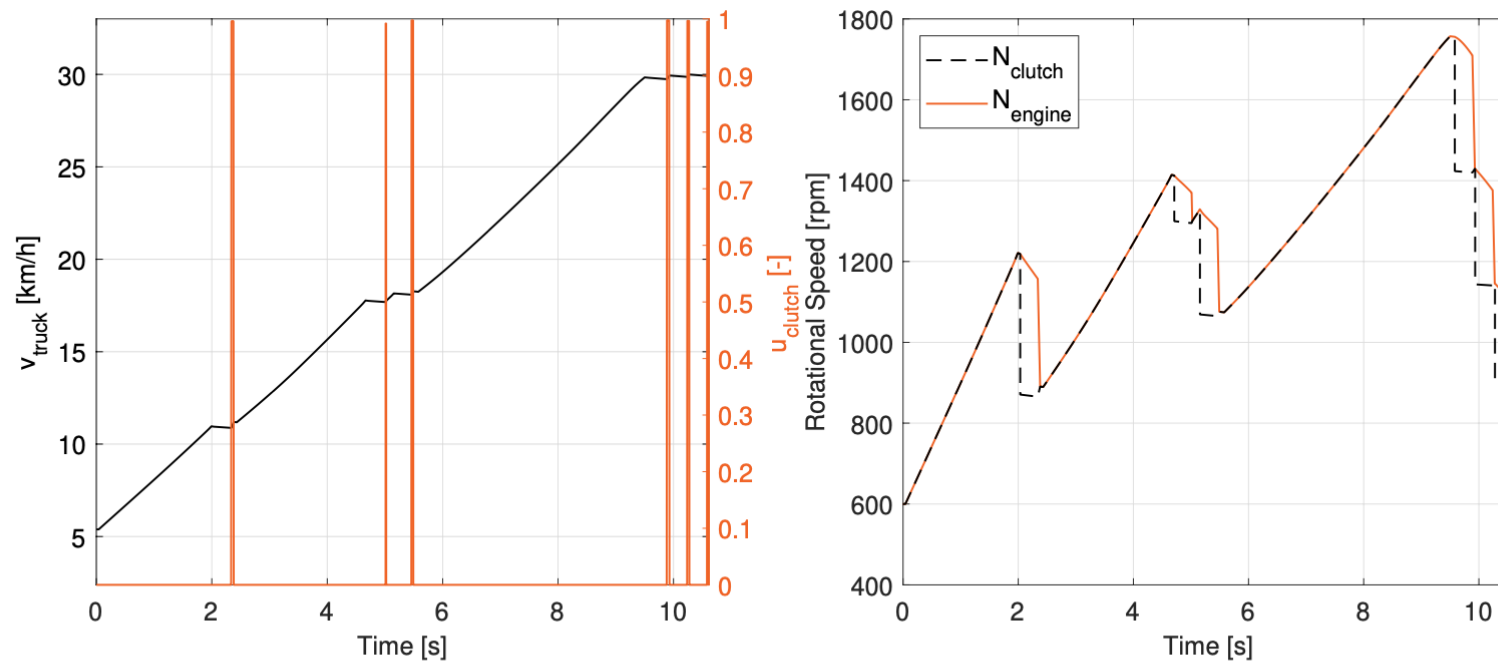


Figure 7.4: Acceleration from 5 to 30 km/h, where all the gears between 4 and 10 has to be used.



# Paper IV – Results – Optimal Gears

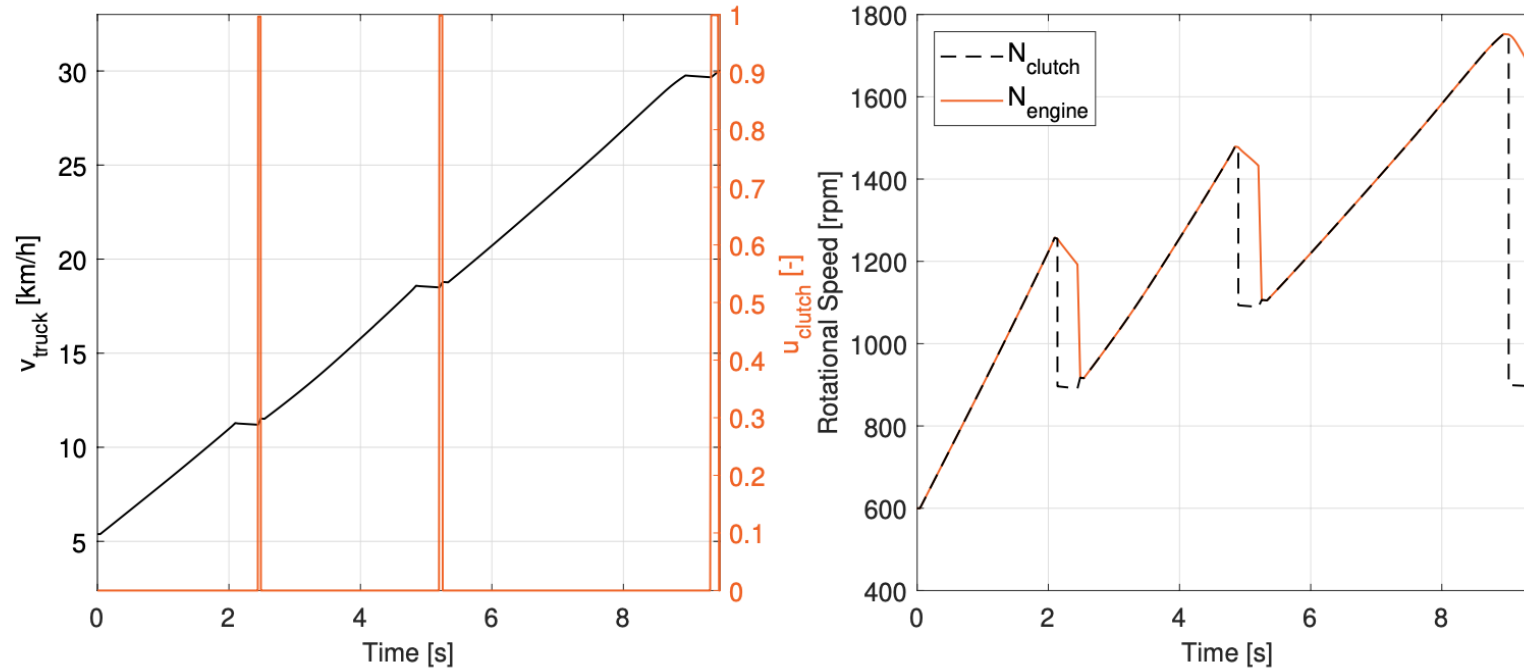


Figure 7.5: Acceleration from 5 to 30 km/h, where the non-used gears are removed from the set of active gears.

# Paper V



## A Comparison of Optimal Gear Shifts for Stiff and Flexible Driveshafts During Accelerations<sup>1</sup>

Kristoffer Ekberg and Lars Eriksson

Department of Electrical Engineering

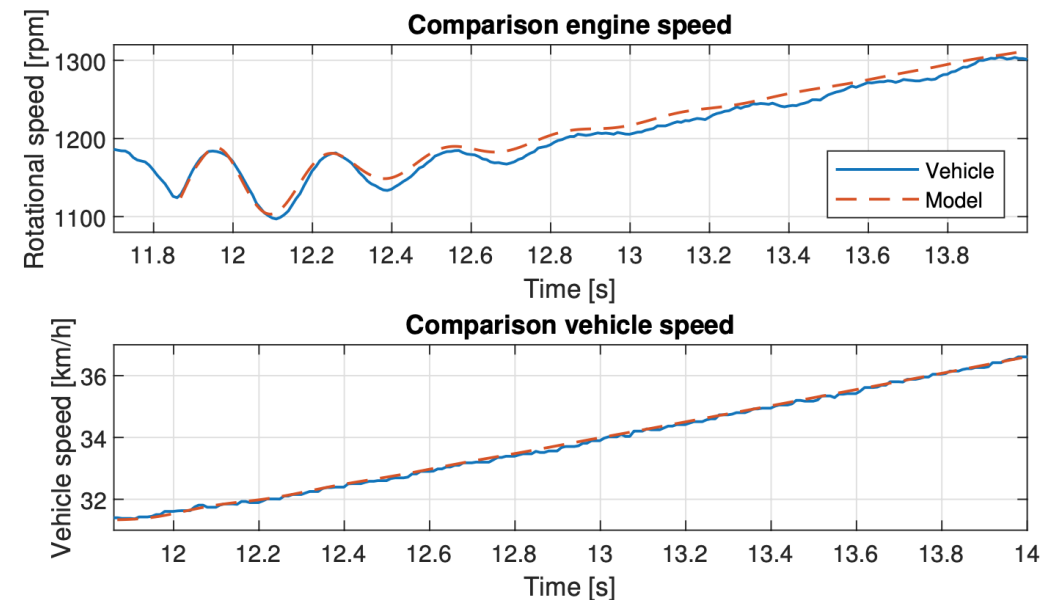
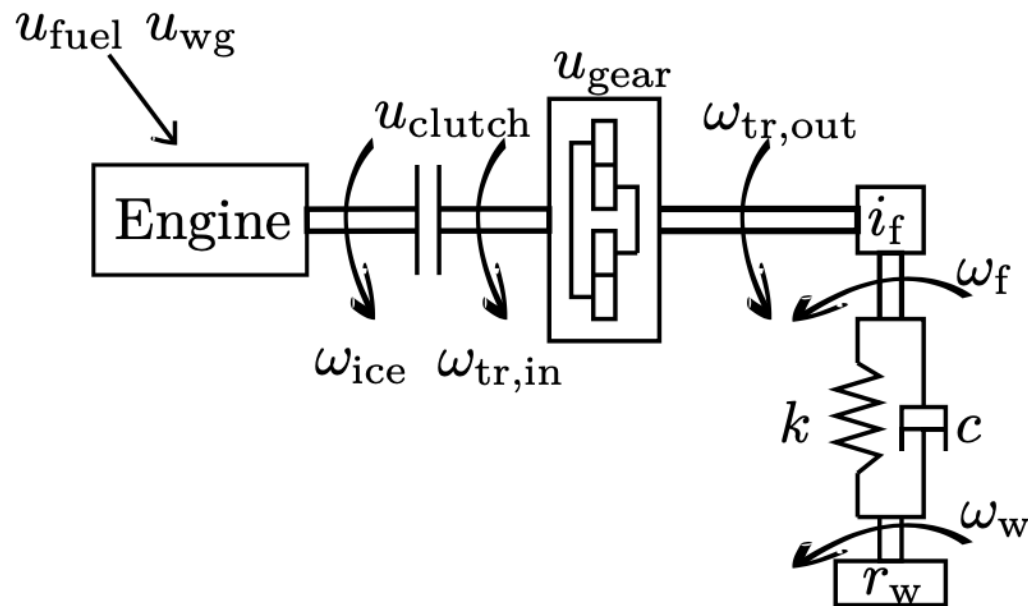
Division of Vehicular Systems

SE-581 83 Linköping, Sweden

<sup>1</sup>Reprinted, with permission, from Kristoffer Ekberg and Lars Eriksson (2020). "A Comparison of Optimal Gear Shifts for Stiff and Flexible Driveshafts During Accelerations." In: *IFAC-PapersOnLine* 53.2. 21th IFAC World Congress, pp. 14413–14419. ISSN: 2405-8963. DOI: <https://doi.org/10.1016/j.ifacol.2020.12.1410>. The formatting is restricted to adjusting the appearance of the text, figures, tables, and the reference style without changing their content.

# Paper V – contribution

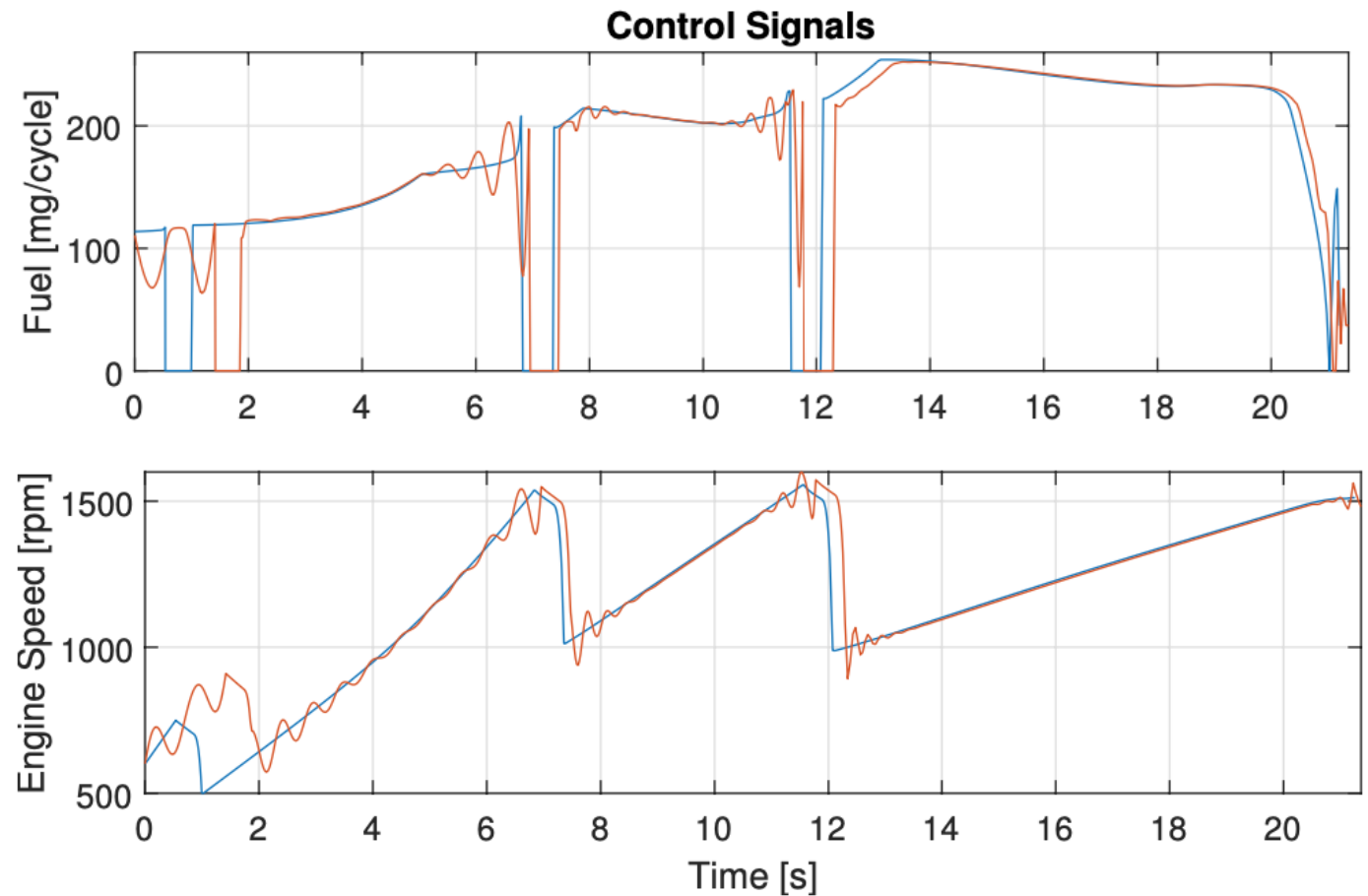
- Impact of a flexible driveshaft when solving acceleration missions for fuel optimal controls



# Paper V – Comparison of the two driveline representations

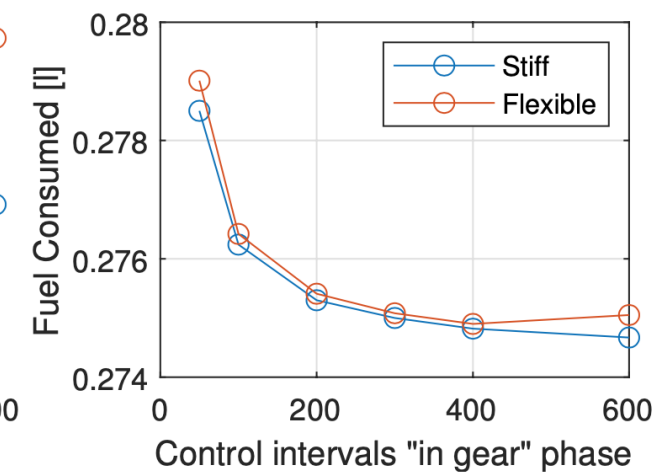
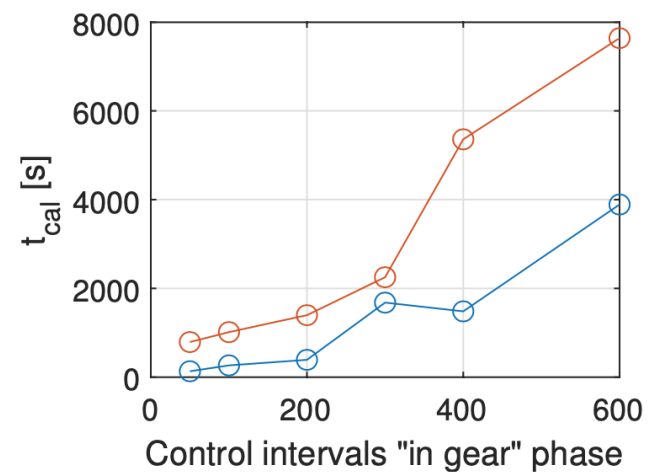
Fuel optimal acceleration

- **Blue:** Stiff driveline
- **Red:** Flexible driveline



# Paper V – Sensitivity Analysis

- Change of control signal intervals “in gear”: resolution of the discretization when formulating the optimal control problem.



# Paper VI



## Electrification of a Heavy-Duty CI Truck—Comparison of Electric Turbocharger and Crank Shaft Motor <sup>1</sup>

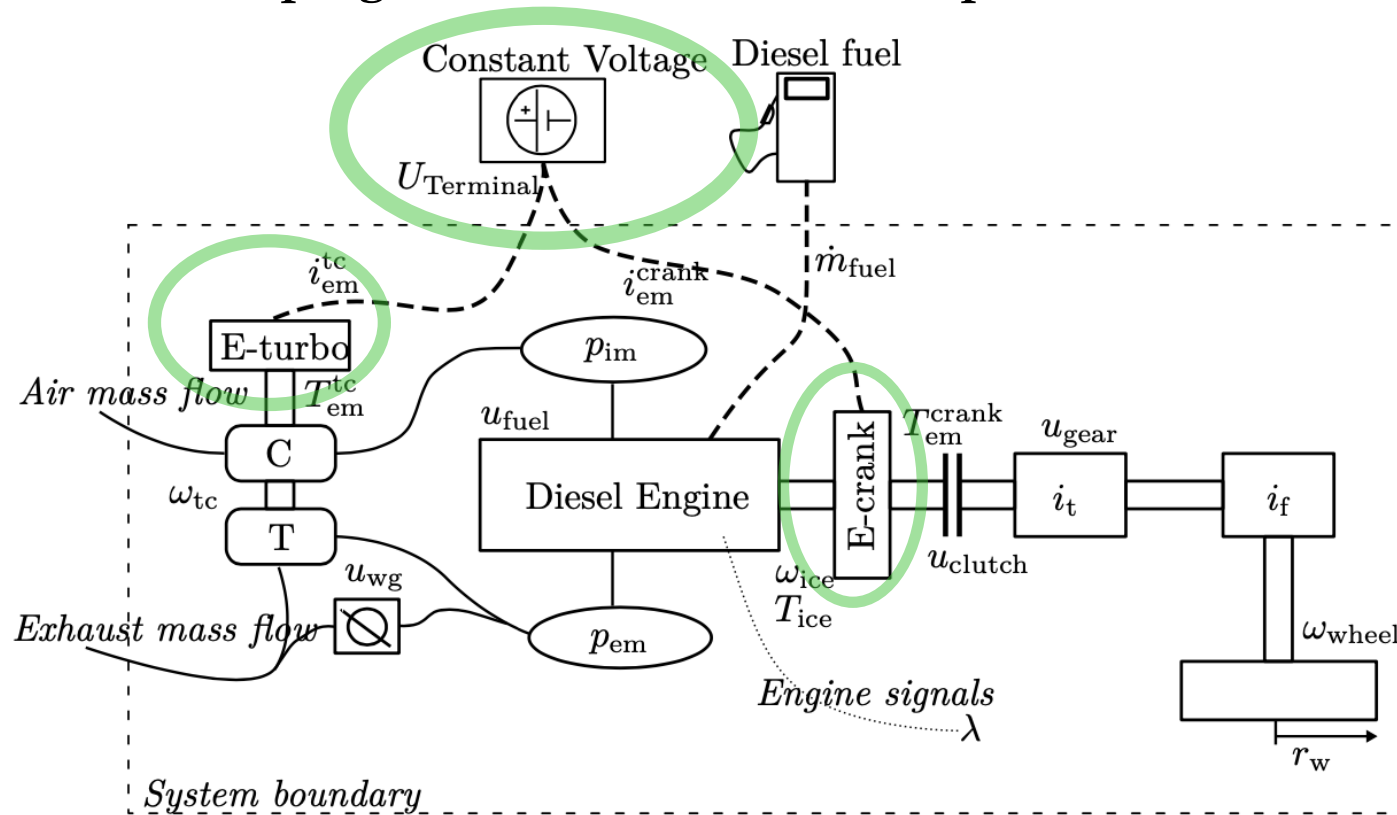
Kristoffer Ekberg, Lars Eriksson, and Christofer Sundström  
Department of Electrical Engineering  
Division of Vehicular Systems  
SE-581 83 Linköping, Sweden

<sup>1</sup>Reprinted, with permission, from Kristoffer Ekberg, Lars Eriksson, and Christofer Sundström (2021). "Electrification of a Heavy-Duty CI Truck—Comparison of Electric Turbocharger and Crank Shaft Motor." In: *Energies* 14.5. Licenced under CC-BY. ISSN: 1996-1073. DOI: [10.3390/en14051402](https://doi.org/10.3390/en14051402). The formatting is restricted to adjusting the appearance of the text, figures, tables, and the reference style without changing their content.

# Paper VI – System Description & Contribution

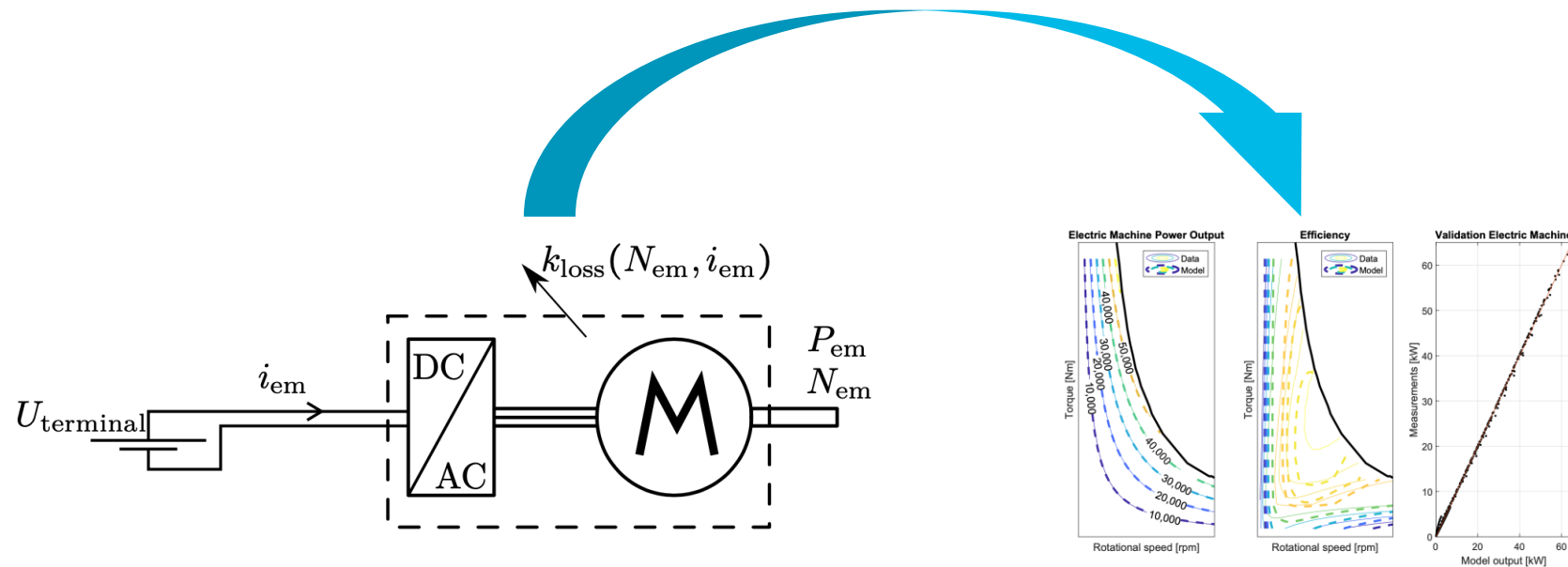
- Developing a method to enable comparisons of electrification architectures

$$J = \dot{m}_{fuel} Q_{LHV} + \beta U_{Terminal} i_{motor}$$



# Paper VI – Electric Motor Model

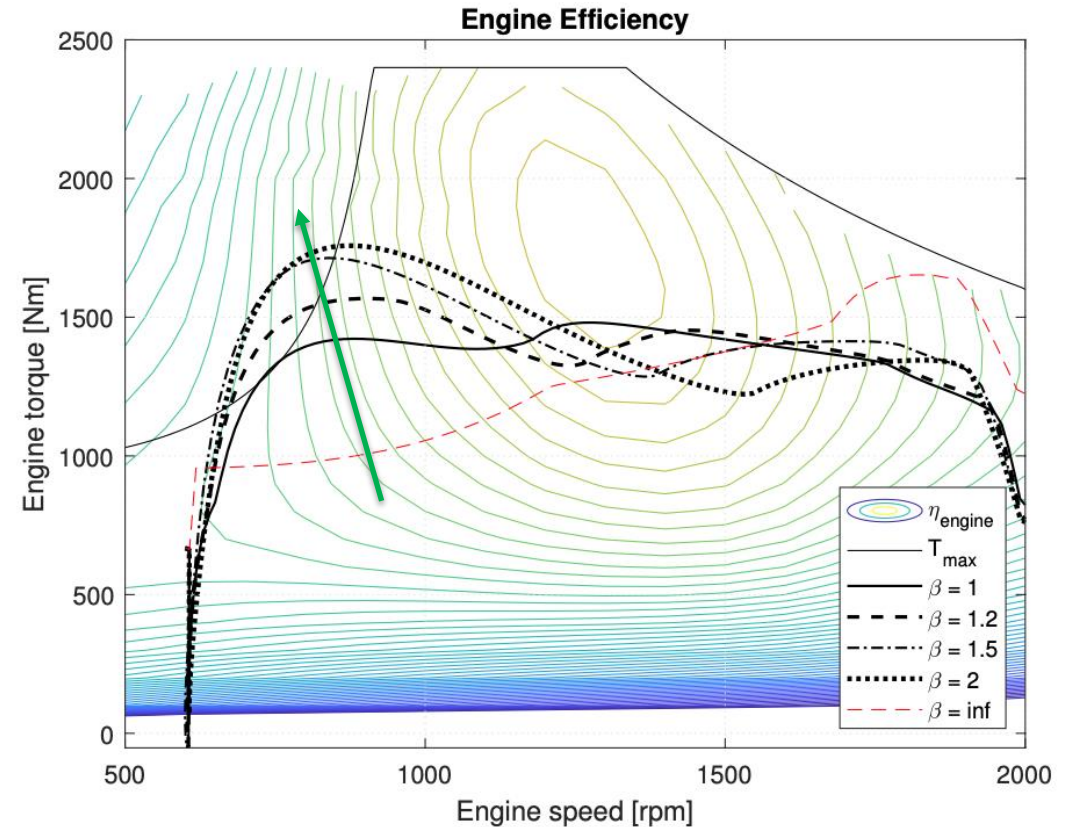
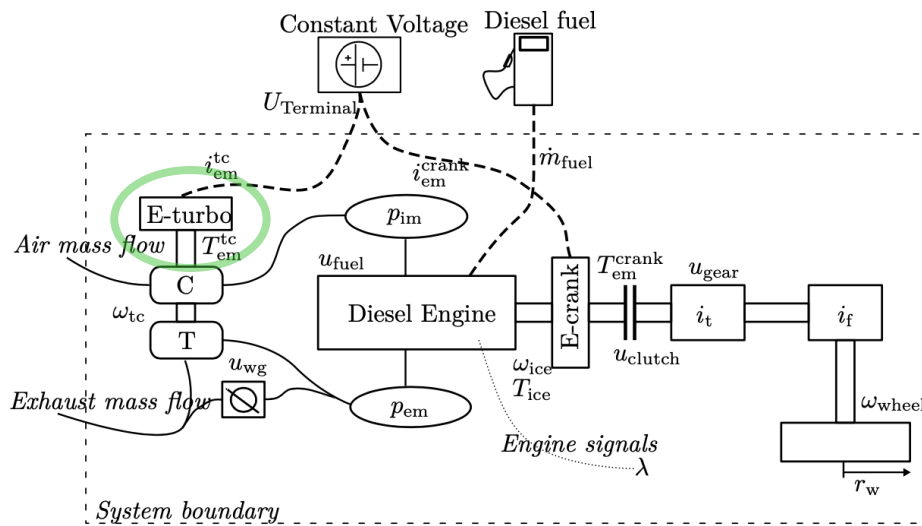
- Development of reference model
- Scaling the model to the size of either propulsion or E-turbo motor.





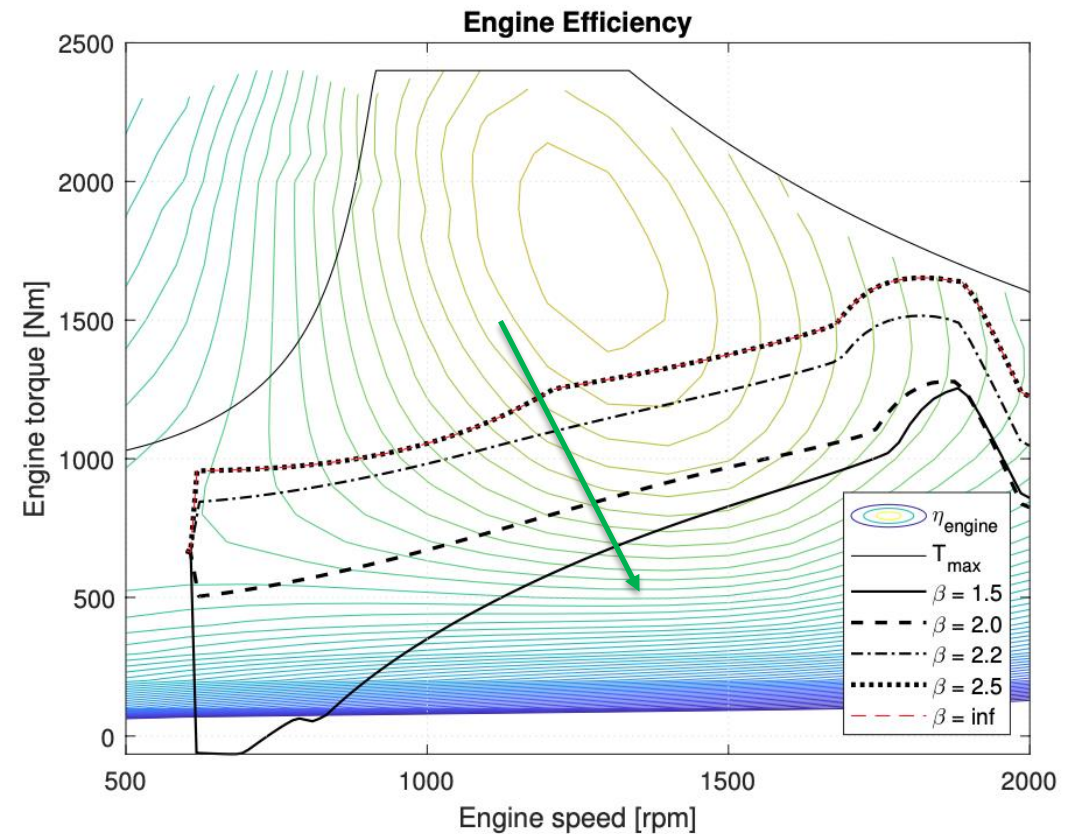
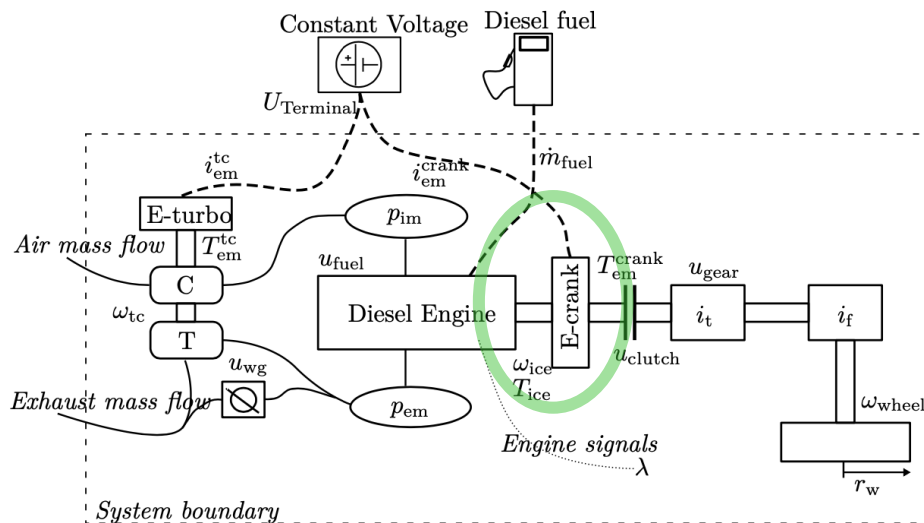
# Paper VI – Electric Turbocharger

- Using the E-turbo results in an increase of output torque at low engine speeds.

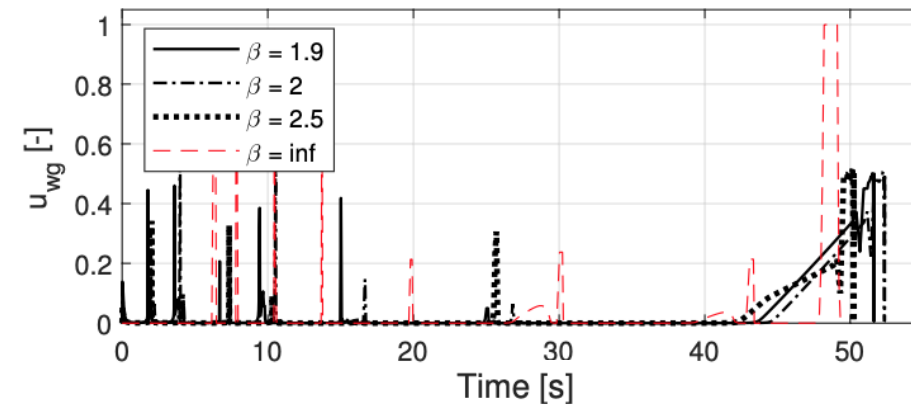
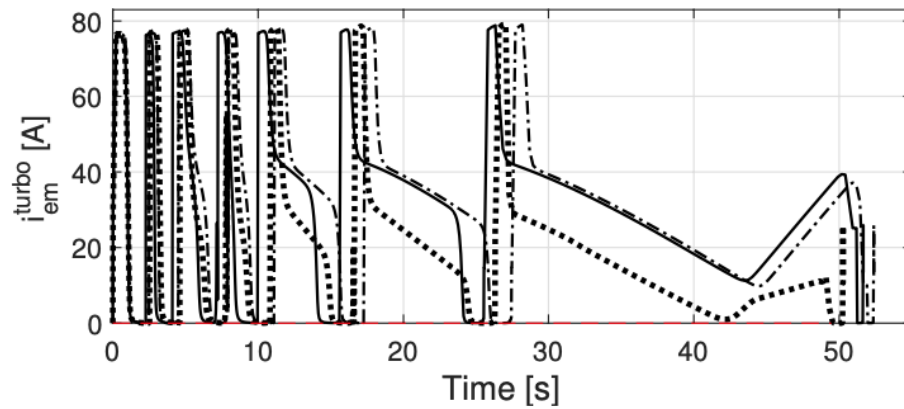
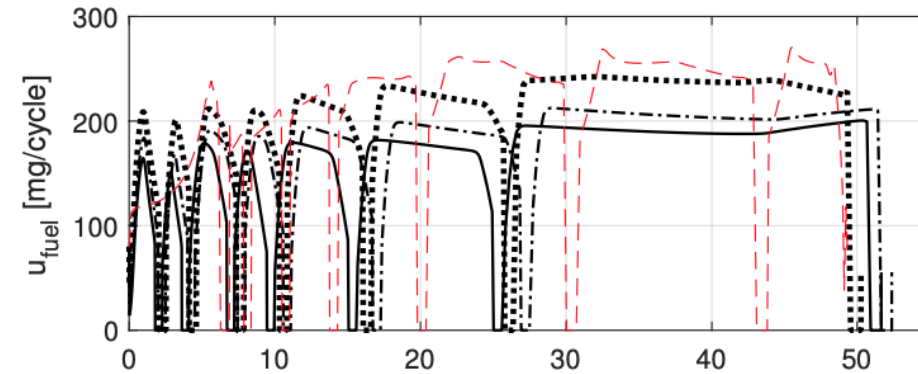
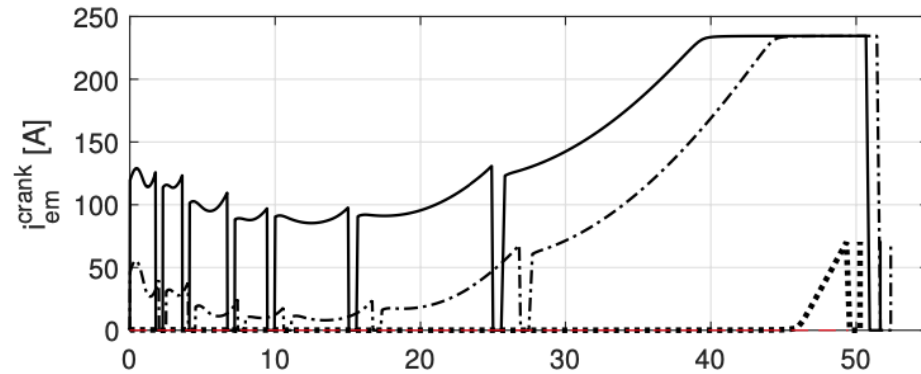


# Paper VI – Electric Crank Shaft Motor

- Using the E-crank results in a reduction of output torque from the diesel engine

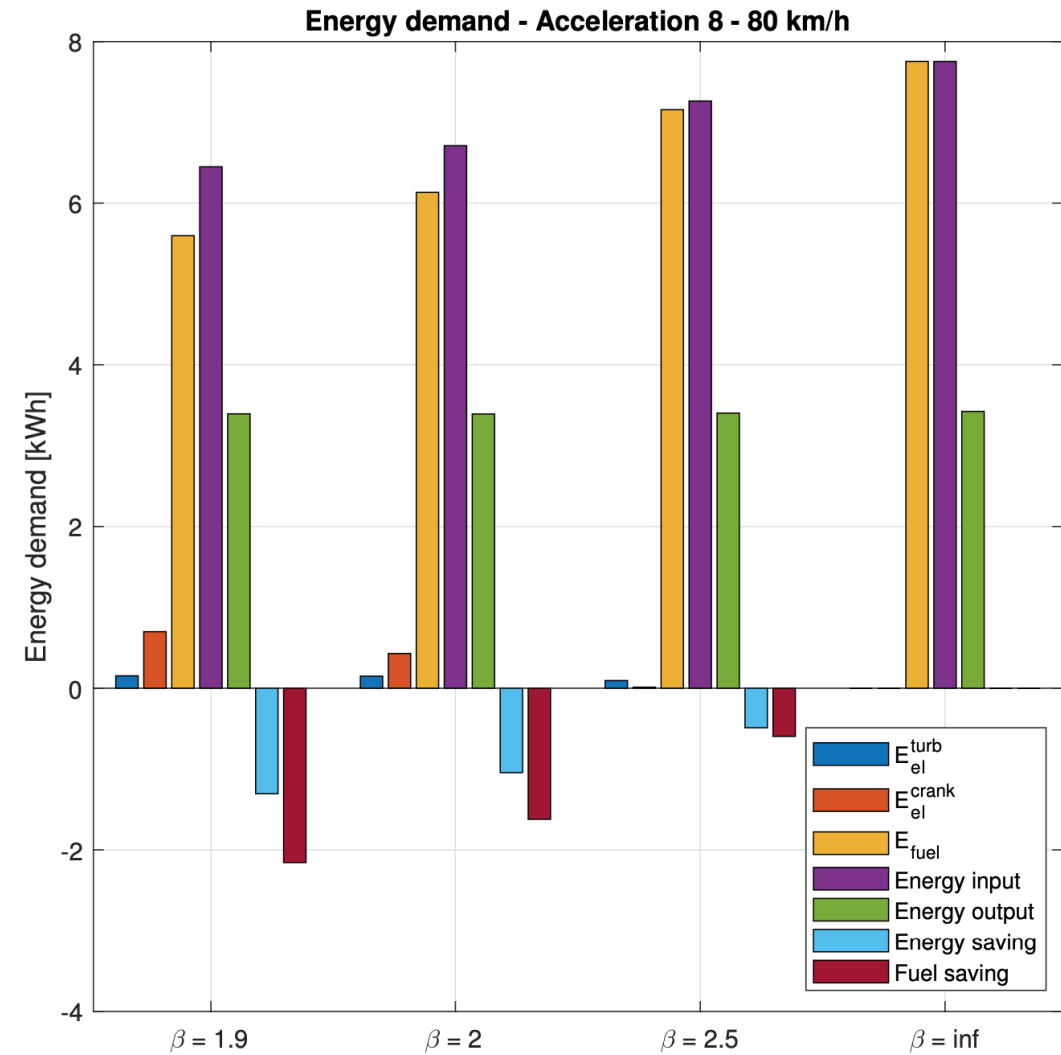


# Paper VI – Acceleration 8-80 km/h



# Paper VI – Consumed Energy

- Lower  $\beta$  – Higher utilization of E-crank
- Higher  $\beta$  – Higher utilization of E-turbo in comparison to E-crank.



# Thesis Contributions

# Thesis Contributions

- Controller for E-turbo
- Turbine model taking speed-lines into account
- Load dependent efficiency model for a CI engine
- Validated MVEM engine model released open source
- Method to investigate gear shifts for fuel optimal accelerations
- Analyzed impact of flexible driveline
- Electric motor model suitable for optimal control
- Optimal power split in HEV with multiple electric motors

# Questions

**Kristoffer Ekberg**  
**Vehicular Systems**  
**Department of Electrical Engineering**  
**Linköping university, Sweden**