

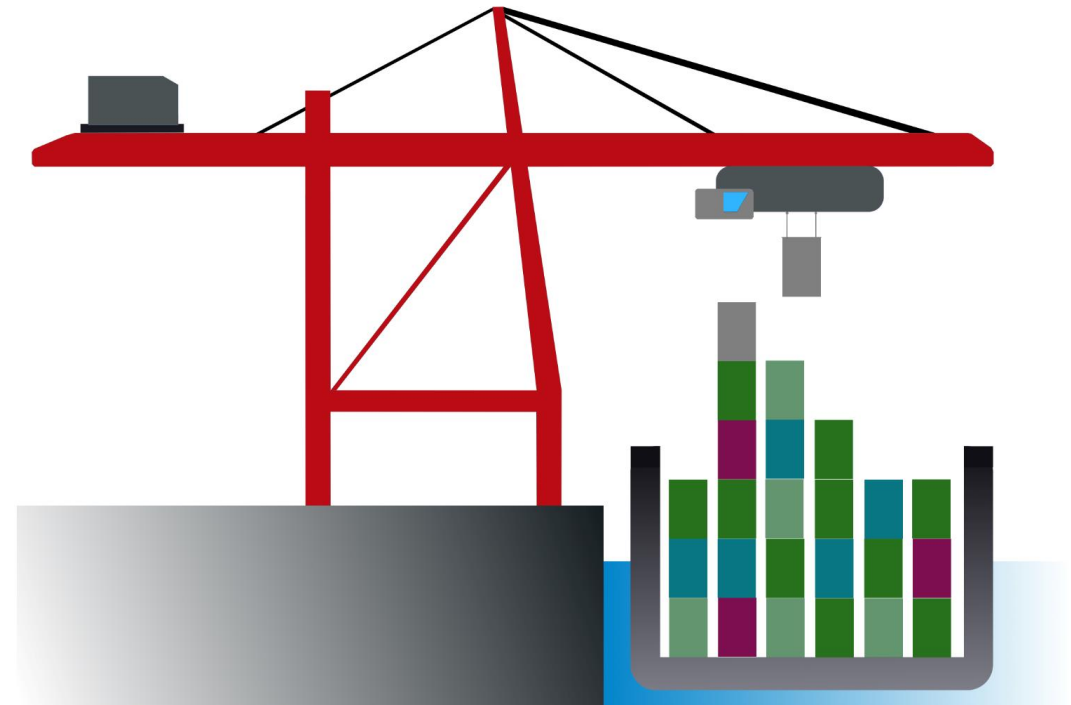
Optimal control of cranes subject to container height constraints

Filipe Marques Barbosa and Johan Löfberg

Loading and unloading ships

Objective: Trade-off time and energy when loading a container ship.

Challenge: Avoid collision with container stacks.



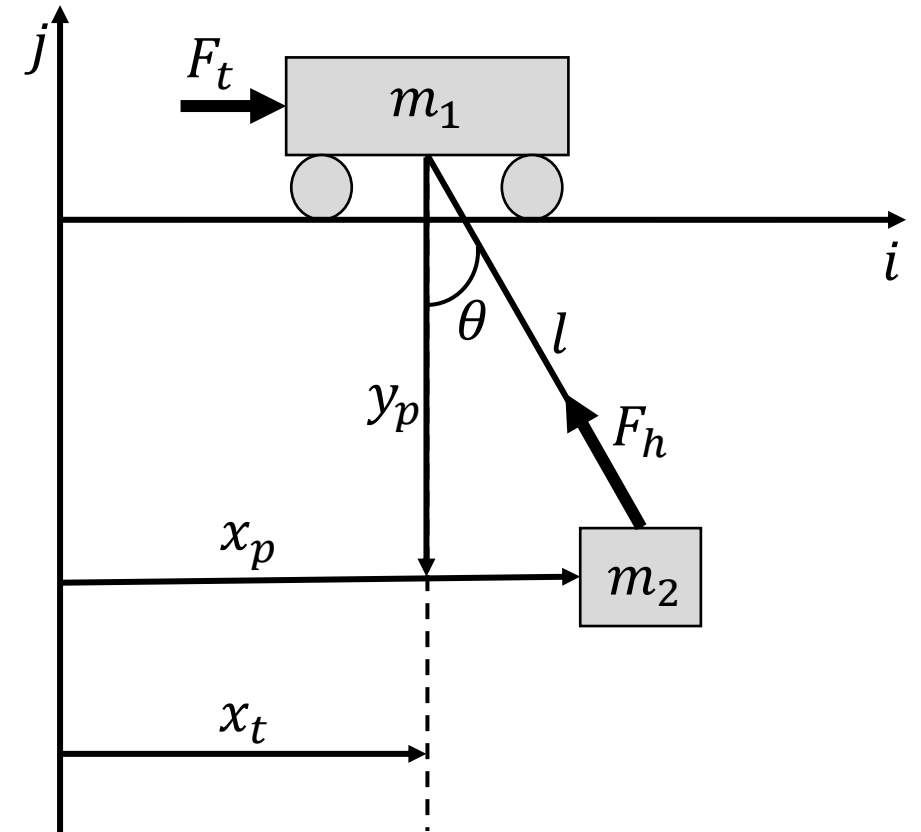
Modelling

First obtain a nonlinear state-space representation of the system

$$\dot{x}(t) = f(t, x(t), u(t)),$$

where the state variables are

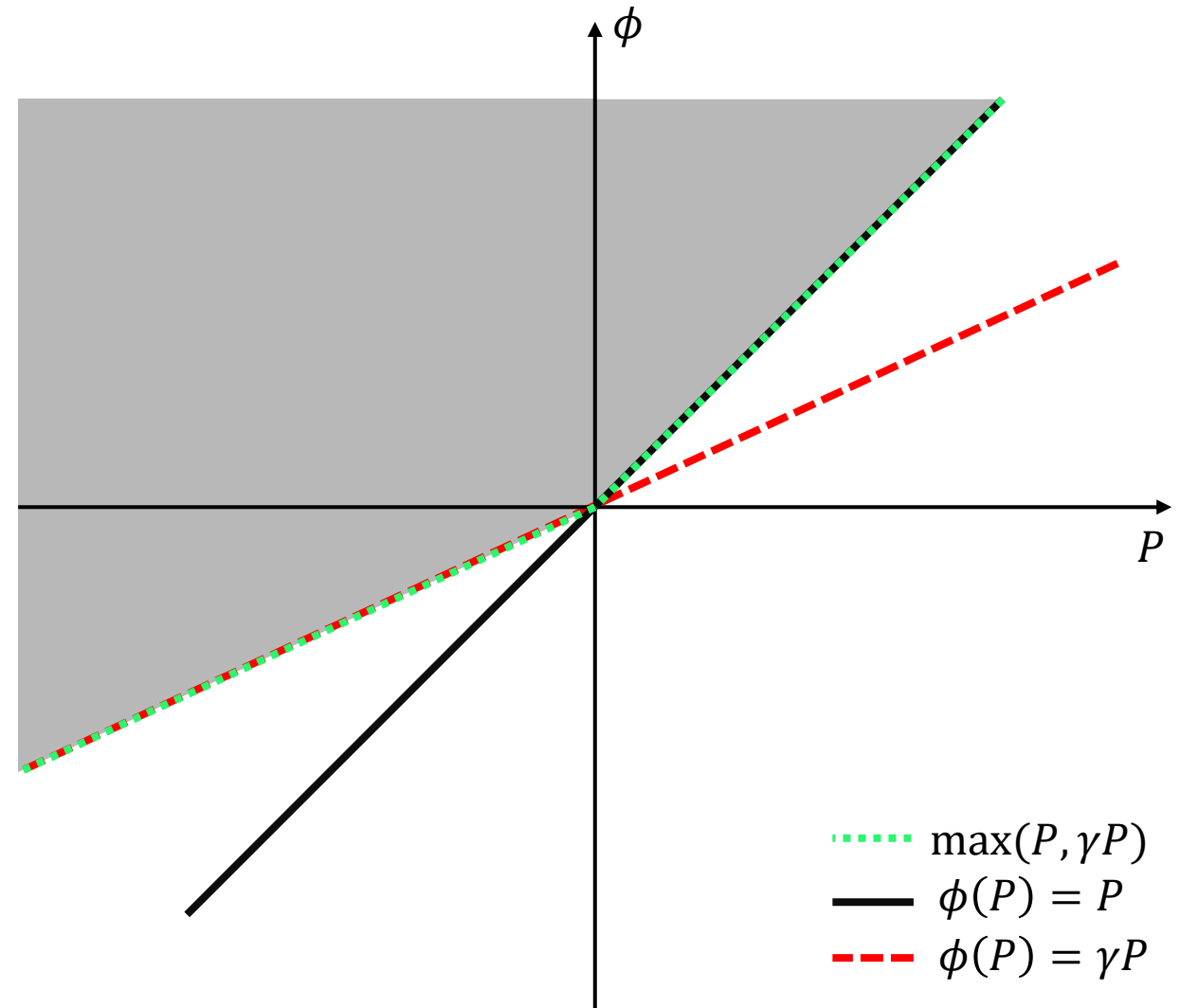
$$x = [x_p, \dot{x}_p, y_p, \dot{y}_p, l, \dot{l}, \theta, \dot{\theta}]^T$$



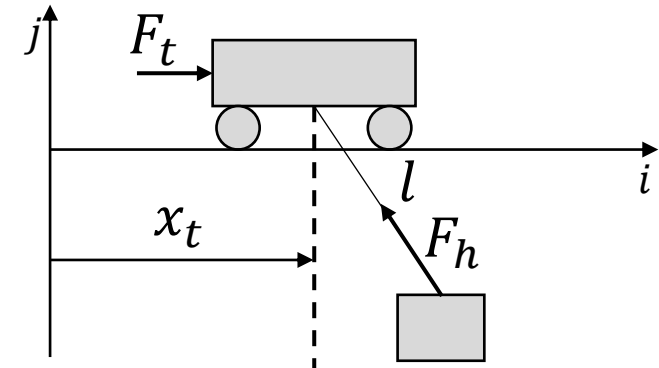
Modelling

If we take energy regeneration into account

$$E(t) = \int_0^t \max(P(\tau), \gamma P(\tau)) d\tau$$



Energy terms



For the STS-crane we consider the energy used to move the trolley and to hoist the payload, so

$$E(t) = \underbrace{\int_0^{t_f} \max(P_t(\tau), \gamma_t P_t(\tau)) d\tau}_{E_t} + \underbrace{\int_0^{t_f} \max(P_h(\tau), \gamma_h P_h(\tau)) d\tau}_{E_h}$$

$$P_t = F_t \dot{x}_t \text{ and } P_h = -F_h \dot{l}$$

Formulation

To avoid a non-smooth integrand, we introduce an auxiliary variable

$$\min_u \int_0^{t_f} \max(P(t), \gamma P(t)) dt \quad \longrightarrow \quad \begin{array}{l} \min_u \int_0^{t_f} z(t) dt \\ \text{s.t. } z(t) \geq P(t) \\ z(t) \geq \gamma P(t) \end{array}$$

Time and energy optimal control

The trade-off between time and energy can be done through

$$\min_u \alpha \int_0^{t_f} dt + (1 - \alpha) \int_0^{t_f} z_t(t) + z_h(t) dt$$

s.t. $\dot{x}(t) = f(t, x(t), u(t))$

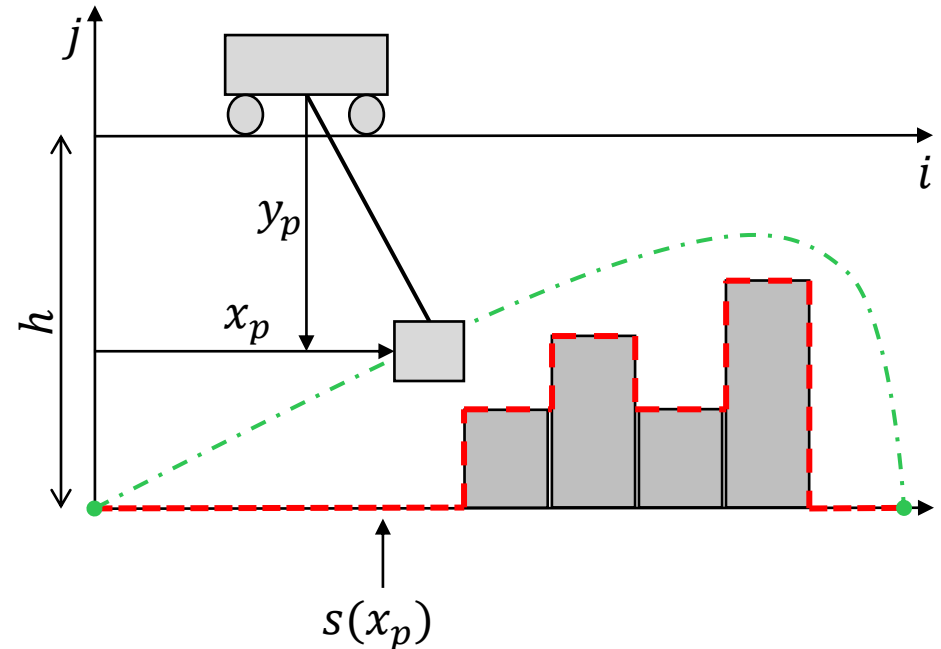
$$z_t(t) \geq P_t(t) \quad z_h(t) \geq P_h(t)$$

$$z_t(t) \geq \gamma P_t(t) \quad z_h(t) \geq \gamma P_h(t)$$

$$0 \leq y_p(t) \leq h - s(x_p(t)) \quad \leftarrow \text{avoidance constraints}$$

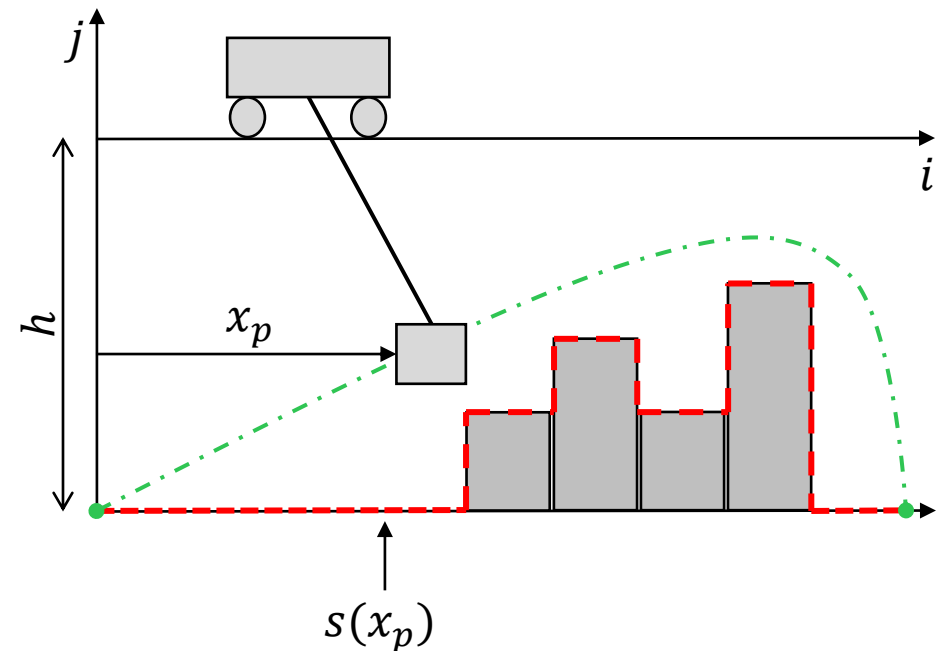
$$\vdots$$

other constraints



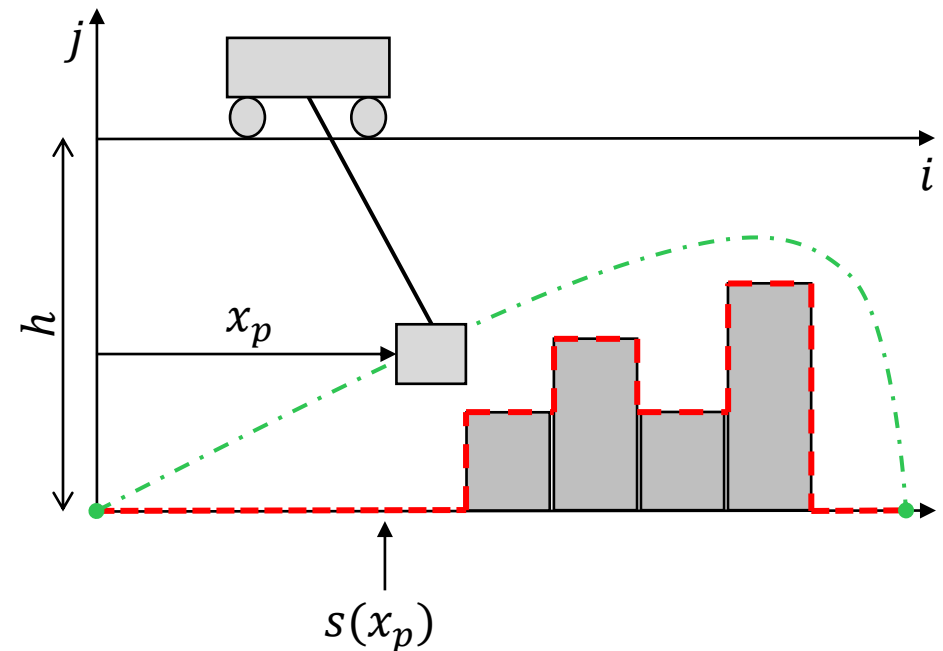
Issues with this formulation

- The constraints need to be constructed from a function $s(x_p(t))$.
- Container height constraints are usually nonlinear and non-smooth function of space.



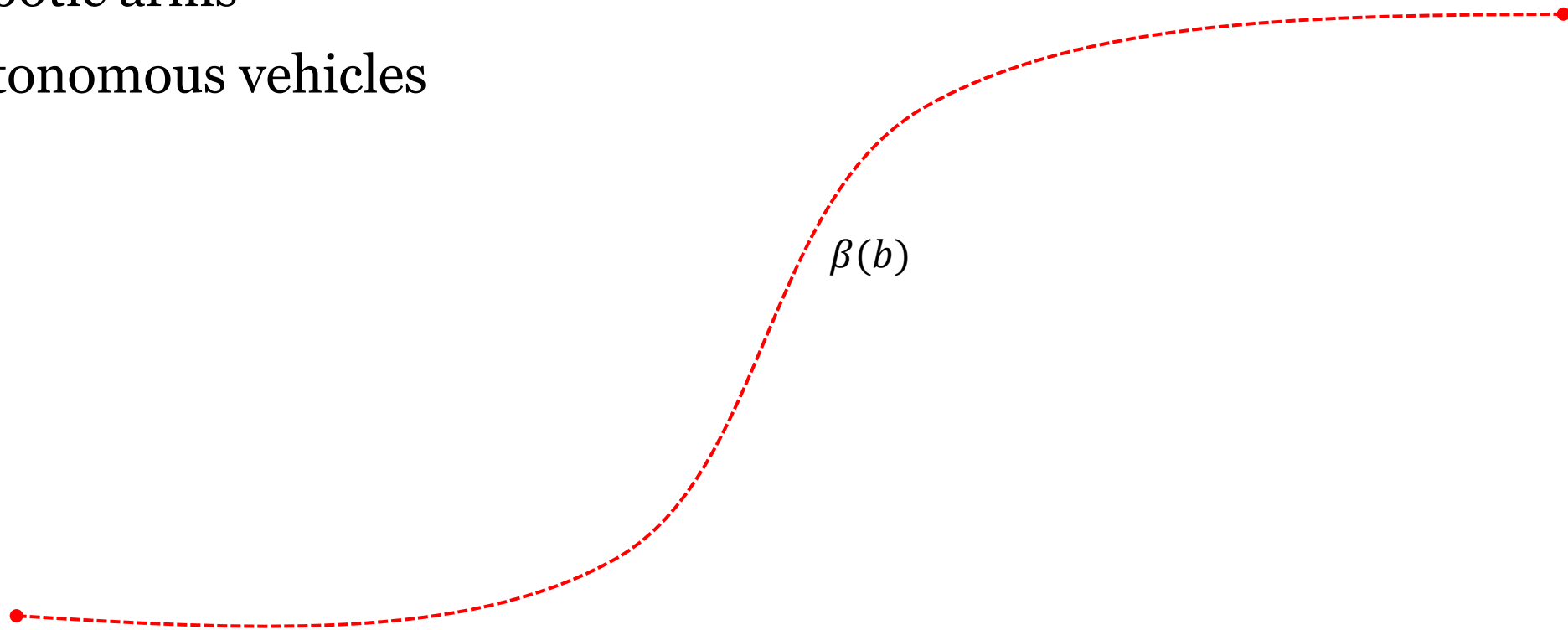
Issues with this formulation

- The stack height at t^k is a function $s(x_p(t^k))$, thus $s(x_p(t))$ must be defined from the current configuration.
- The free variable is also the one being optimized. So, the solution will be influenced by fixed time sampling rate (fixed # of control intervals).



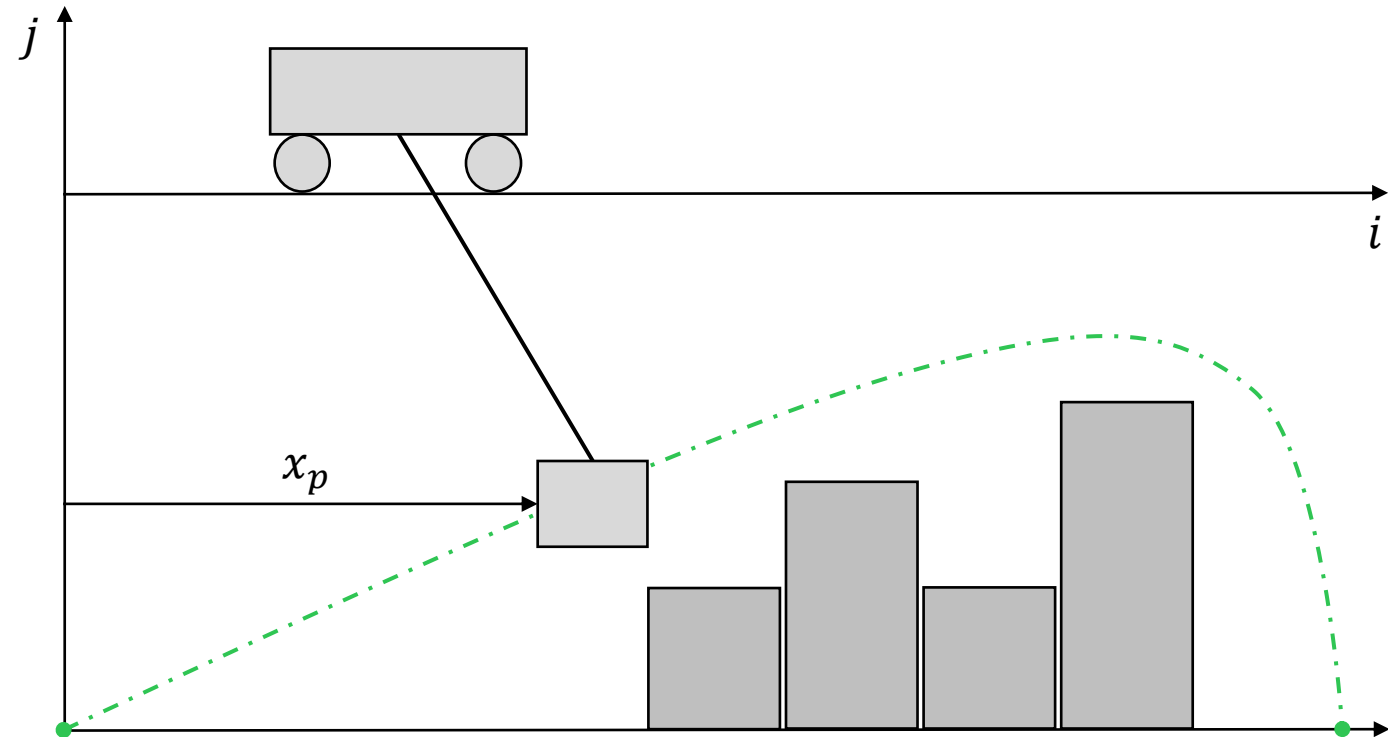
Geometric path

- Robotic arms
- Autonomous vehicles



Geometric path

- Container avoidance



Problem reformulation

Container avoidance constraints are easier described along loading site (x_p).

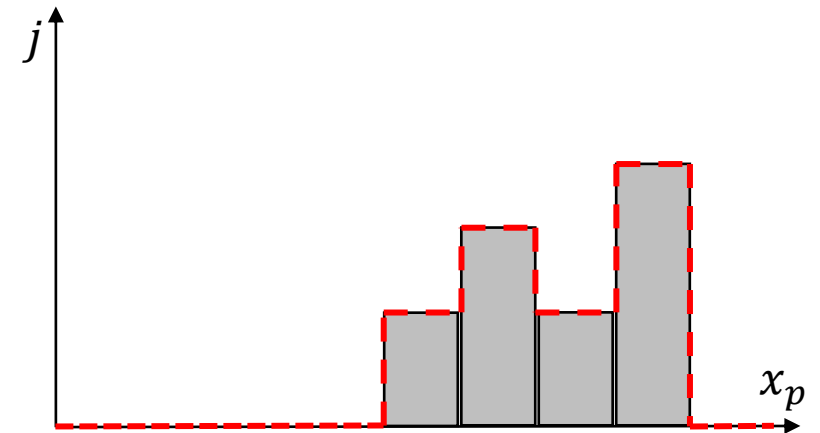
Thus, we change the integration variable

$$\dot{x}_1 = \frac{dx_1}{dt} = x_2 \Rightarrow \frac{dt}{dx_1} = \frac{1}{x_2}, \frac{dx_2}{dx_1} = \dots$$

and

$$x = [t, x'_p, y_p, y'_p, l, l', \theta, \theta']^T$$

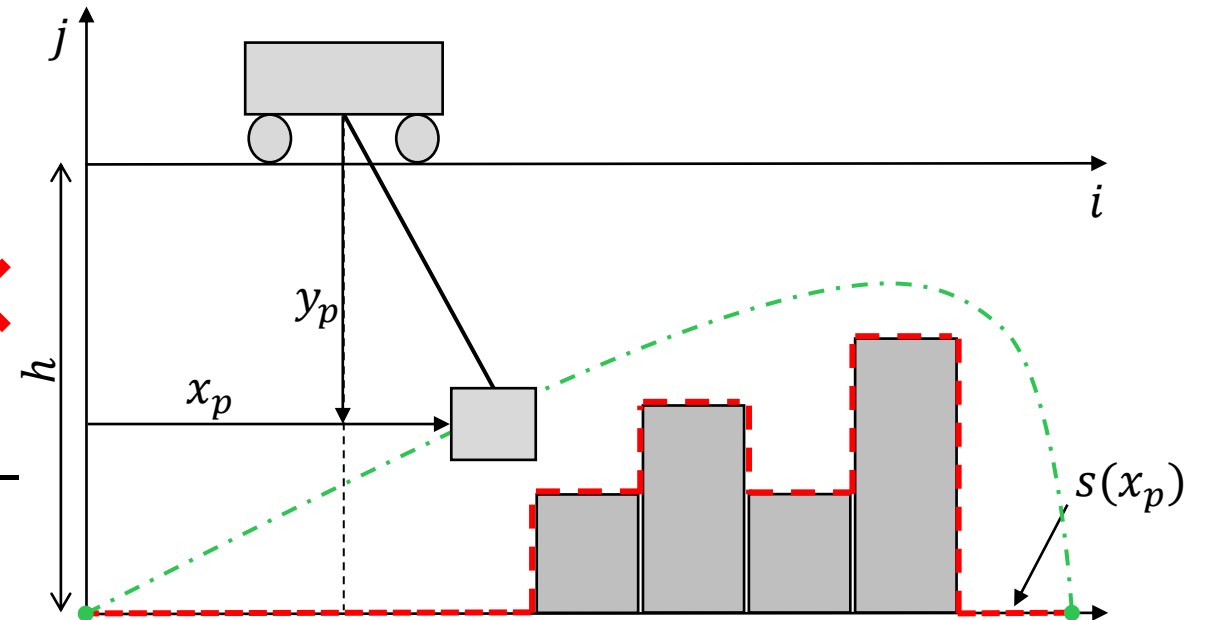
Note: $x' = \frac{dx}{dx_p}$



Geometric constraints

- Time discretization before the variable change leads to

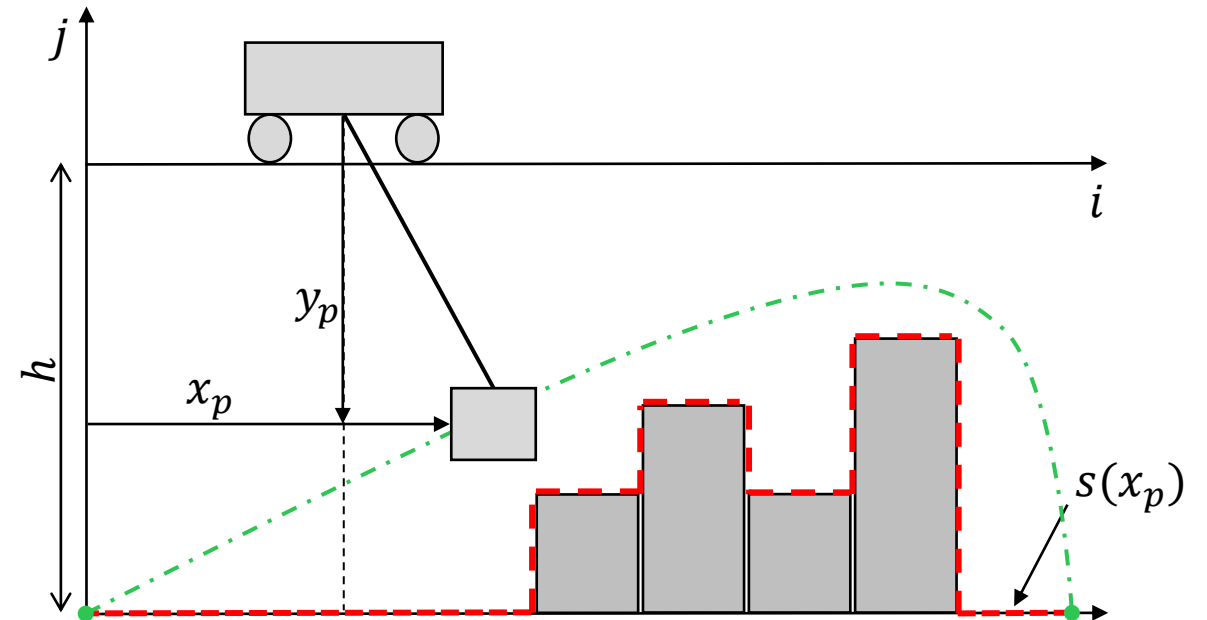
$$0 \leq y_p(x_p(t^k)) \leq h - s(x_p(t^k)). \quad \times$$
- Where $s(x_p)$ is generally discontinuous, nonlinear and non-convex



Geometric constraints

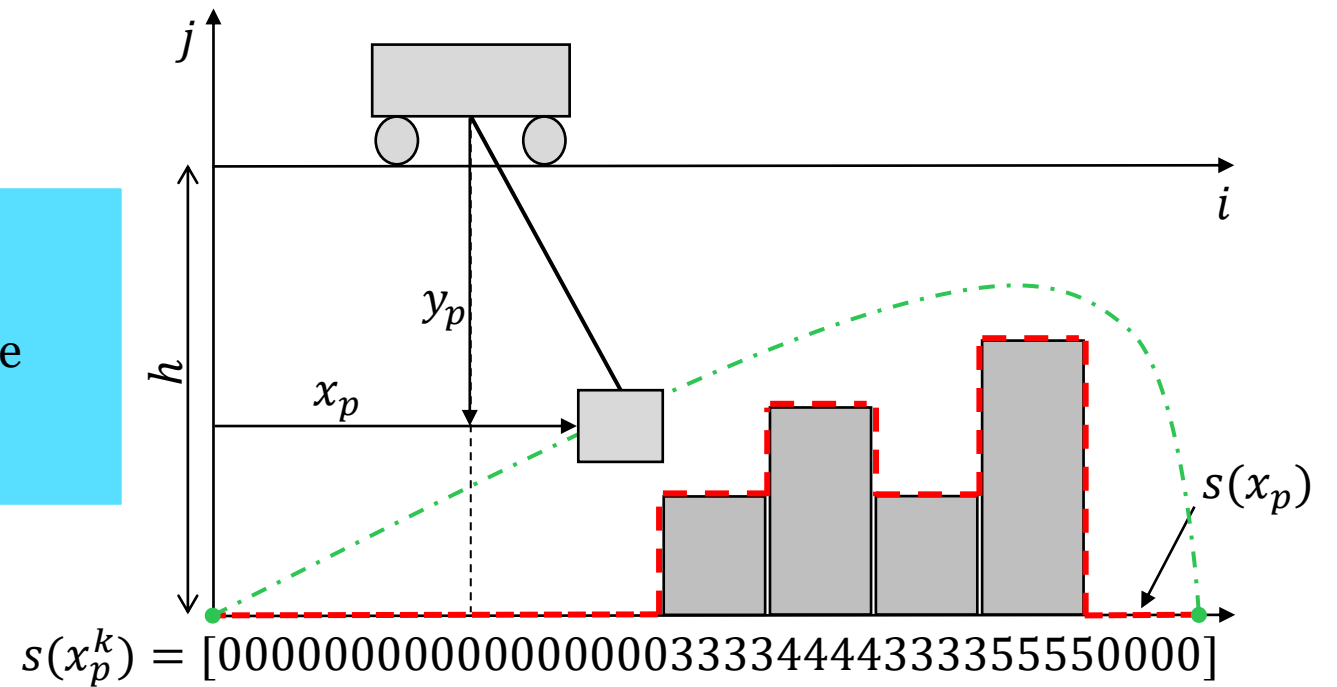
Spatial discretization leads to upper bound constraints in $y_p(x_p)$

$$0 \leq y_p(x_p^k) \leq h - s(x_p^k). \quad \checkmark$$



Geometric constraints

Note that we no longer need an explicit function $s(x_p)$, but simply function values which can be computed when setting up the numerical model.



Additional implications

- A natural choice of the cost function would be

$$J = \alpha \int_{x_{p0}}^{x_{pf}} \frac{1}{x_2} dx_p + (1 - \alpha) \int_{x_{p0}}^{x_{pf}} \frac{z_t(x_p) + z_h(x_p)}{x_2} dx_p,$$

However, $x_1(x_p) = t$ and

$$x_2 x'_9 = z_t(x_p) \Rightarrow x_9(x_p) = \int_{x_{p0}}^{x_{pf}} \frac{z_t(x_p)}{x_2} dx_p$$

$$x_2 x'_{10} = z_h(x_p) \Rightarrow x_{10}(x_p) = \int_{x_{p0}}^{x_{pf}} \frac{z_h(x_p)}{x_2} dx_p$$

Additional implications

- Then...

$$J = \alpha x_1(x_{p_f}) + (1 - \alpha) (x_9(x_{p_f}) + x_{10}(x_{p_f}))$$

New formulation

$$\min_u \quad \alpha \int_0^{t_f} dt + (1 - \alpha) \int_0^{t_f} z_t(t) + z_h(t) dt$$

$$\text{s.t.} \quad \dot{x}(t) = f(t, x(t), u(t))$$

$$z_t(t) \geq P_t(t) \quad z_h(t) \geq P_h(t)$$

$$z_t(t) \geq \gamma_t P_t(t) \quad z_h(t) \geq \gamma_h P_h(t)$$

$$0 \leq y_p(t) \leq h - s(x_p(t))$$

$$\vdots$$

other constraints

$$\min_u \quad \alpha x_1(x_{p_f}) + (1 - \alpha) (x_9(x_{p_f}) + x_{10}(x_{p_f}))$$

$$\text{s.t.} \quad x_2 \dot{x}(x_p) = f(x_p, x(x_p), u(x_p))$$

$$z_t(x_p) \geq P_t(x_p) \quad z_h(x_p) \geq P_h(x_p)$$

$$z_t(x_p) \geq \gamma_t P_t(x_p) \quad z_h(x_p) \geq \gamma_h P_h(x_p)$$

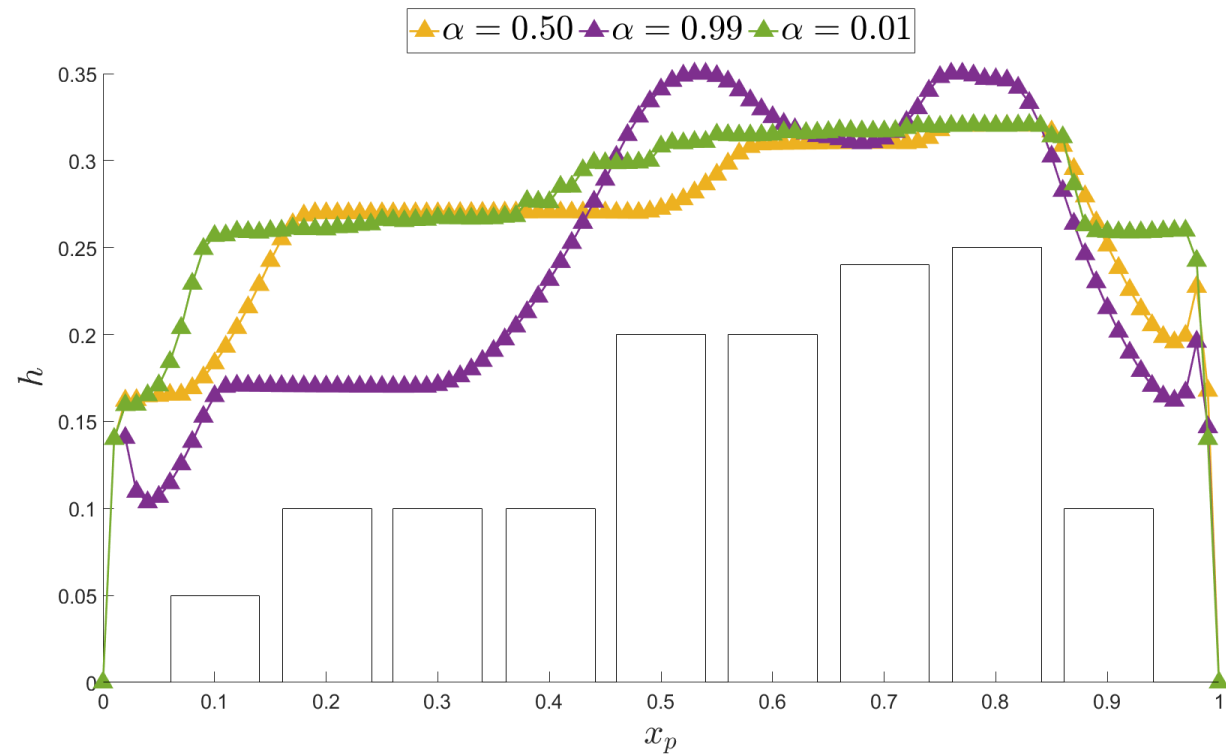
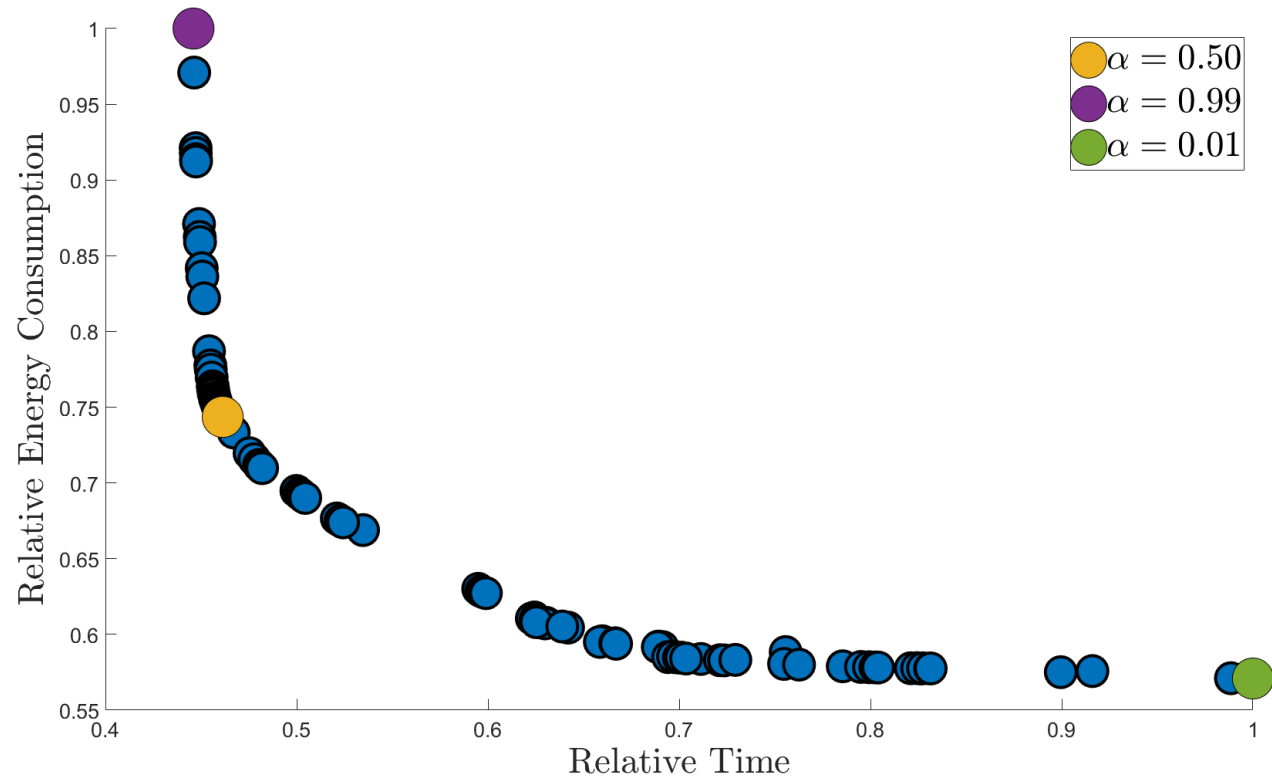
$$0 \leq y_p(x_p) \leq h - s(x_p(x_p))$$

$$\vdots$$

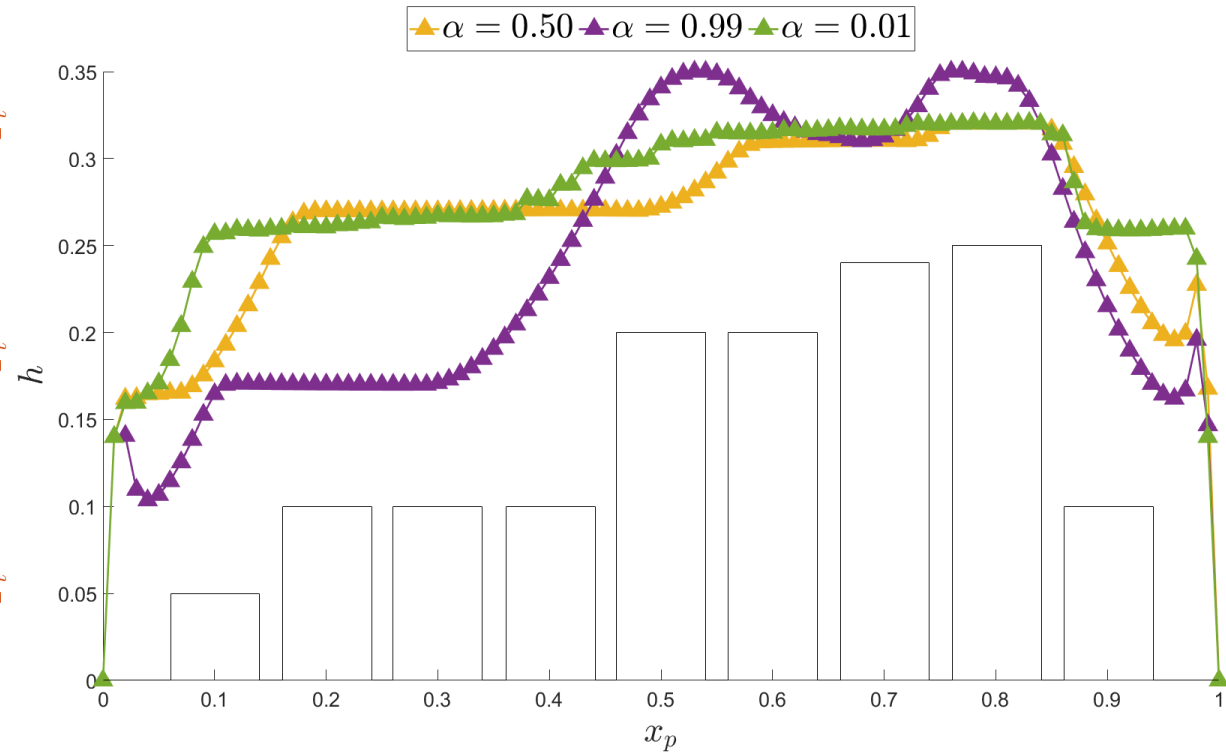
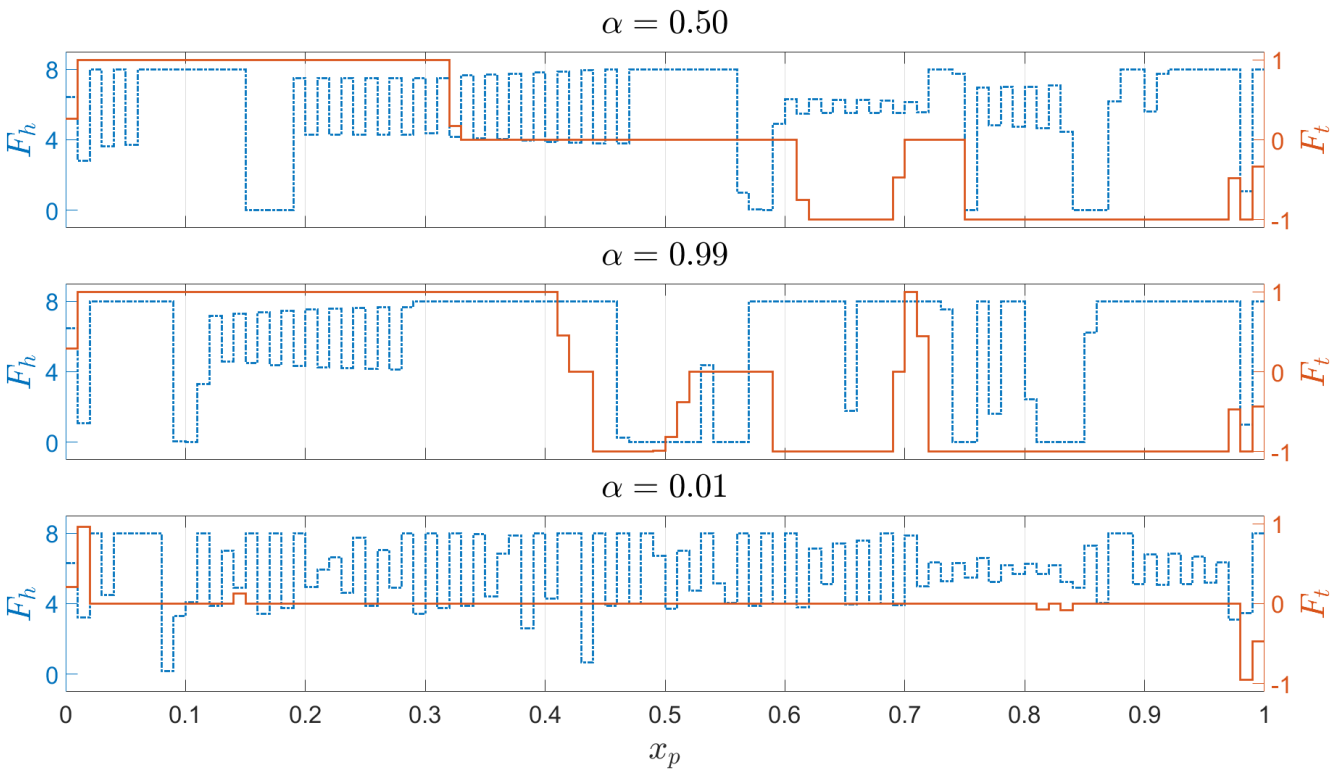
other constraints

← avoidance
constraints →

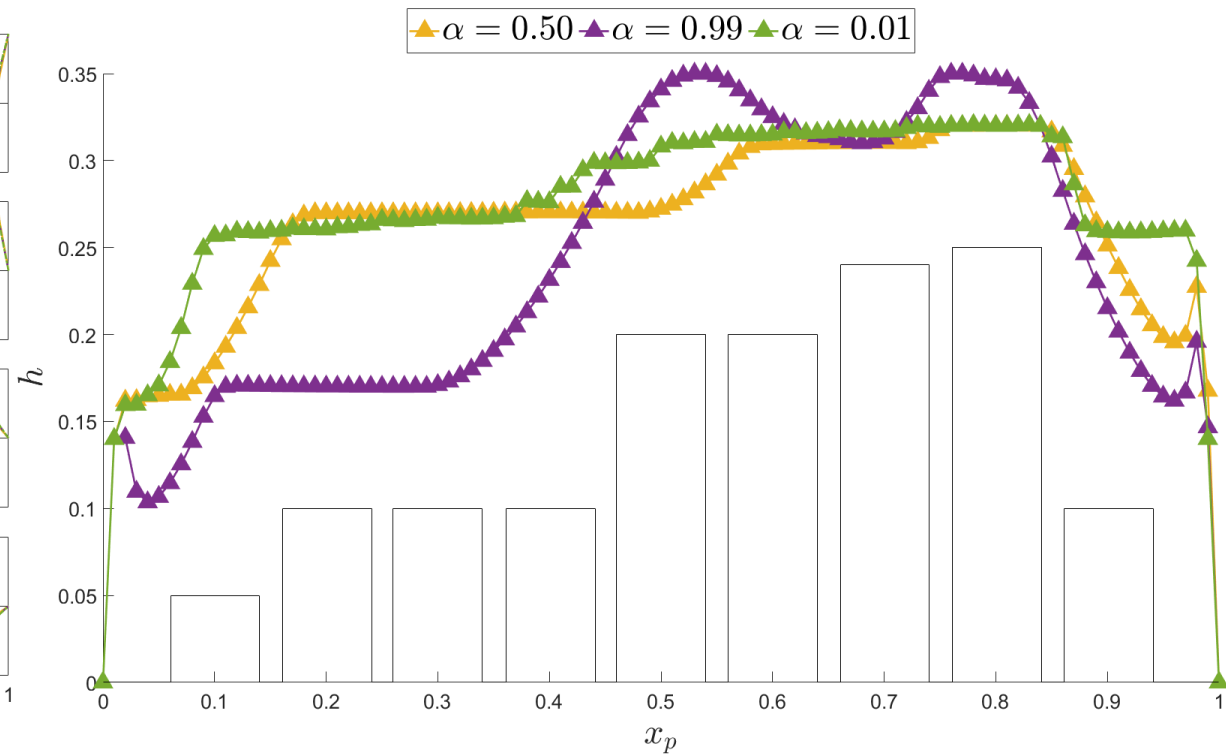
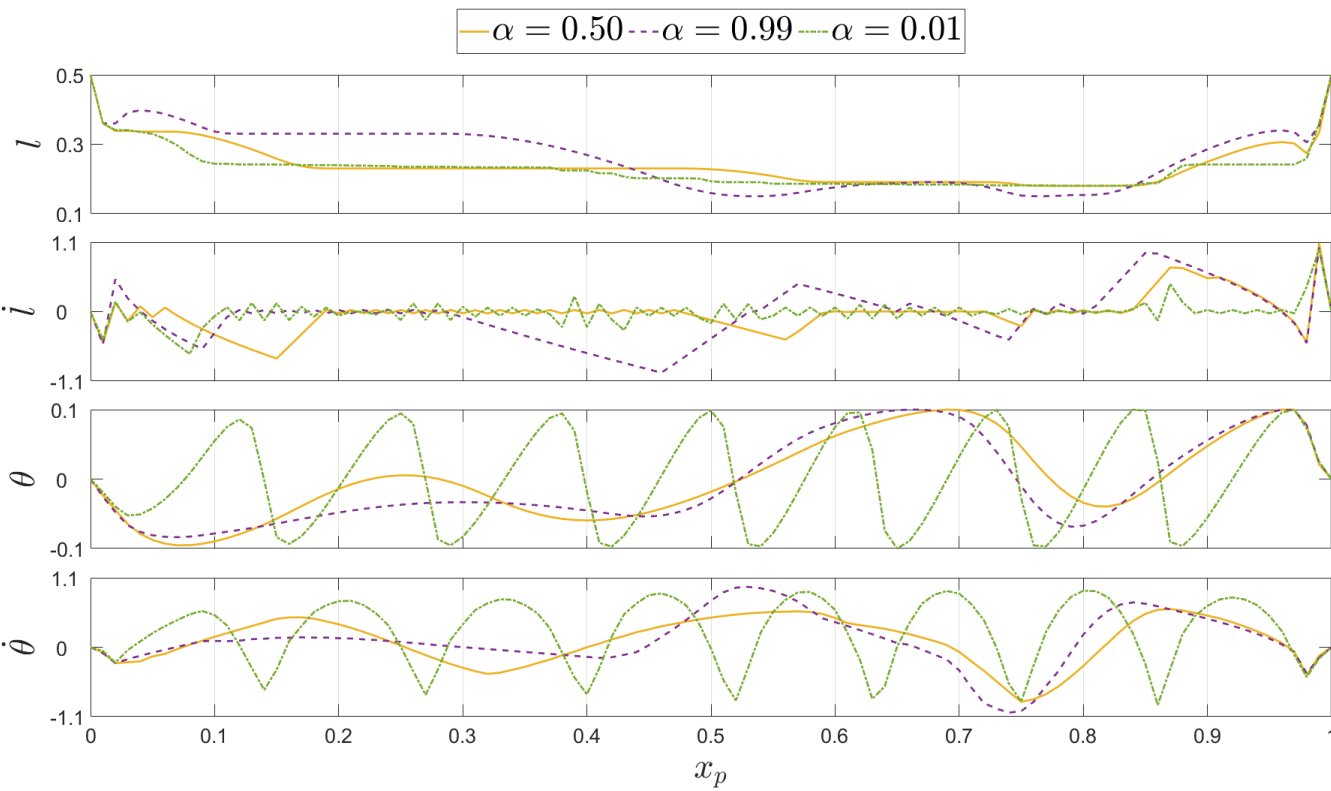
Example



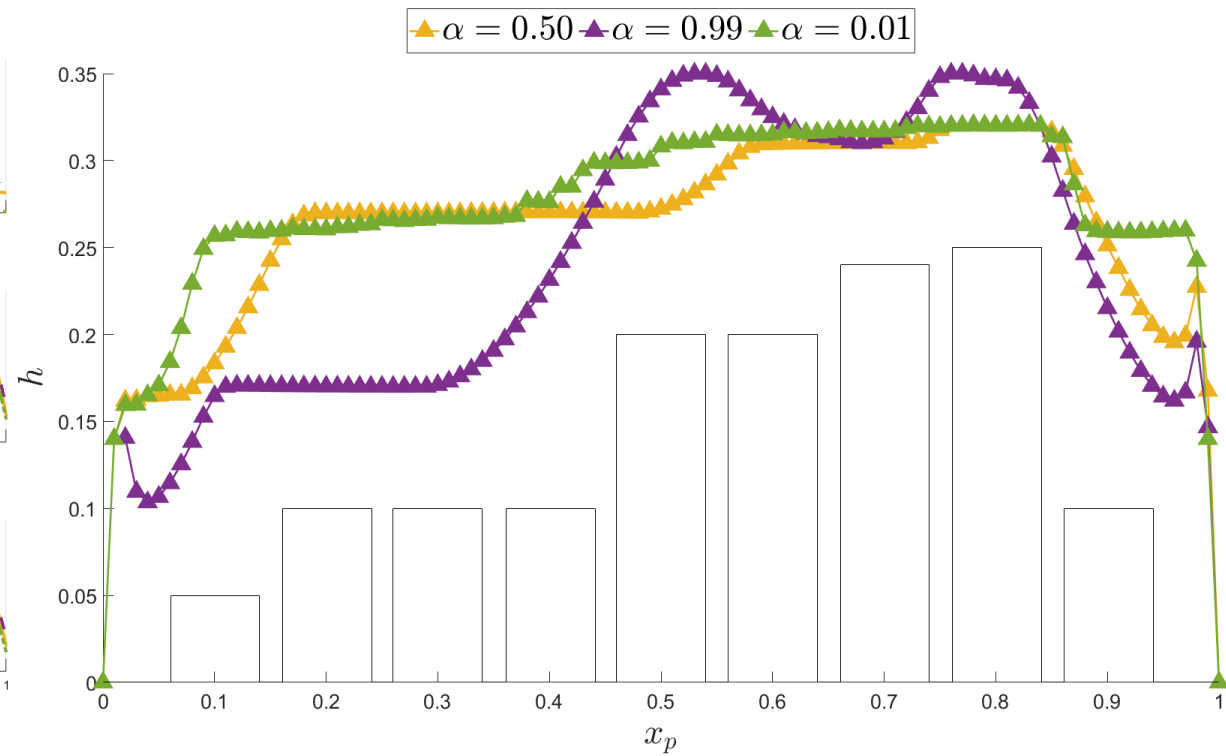
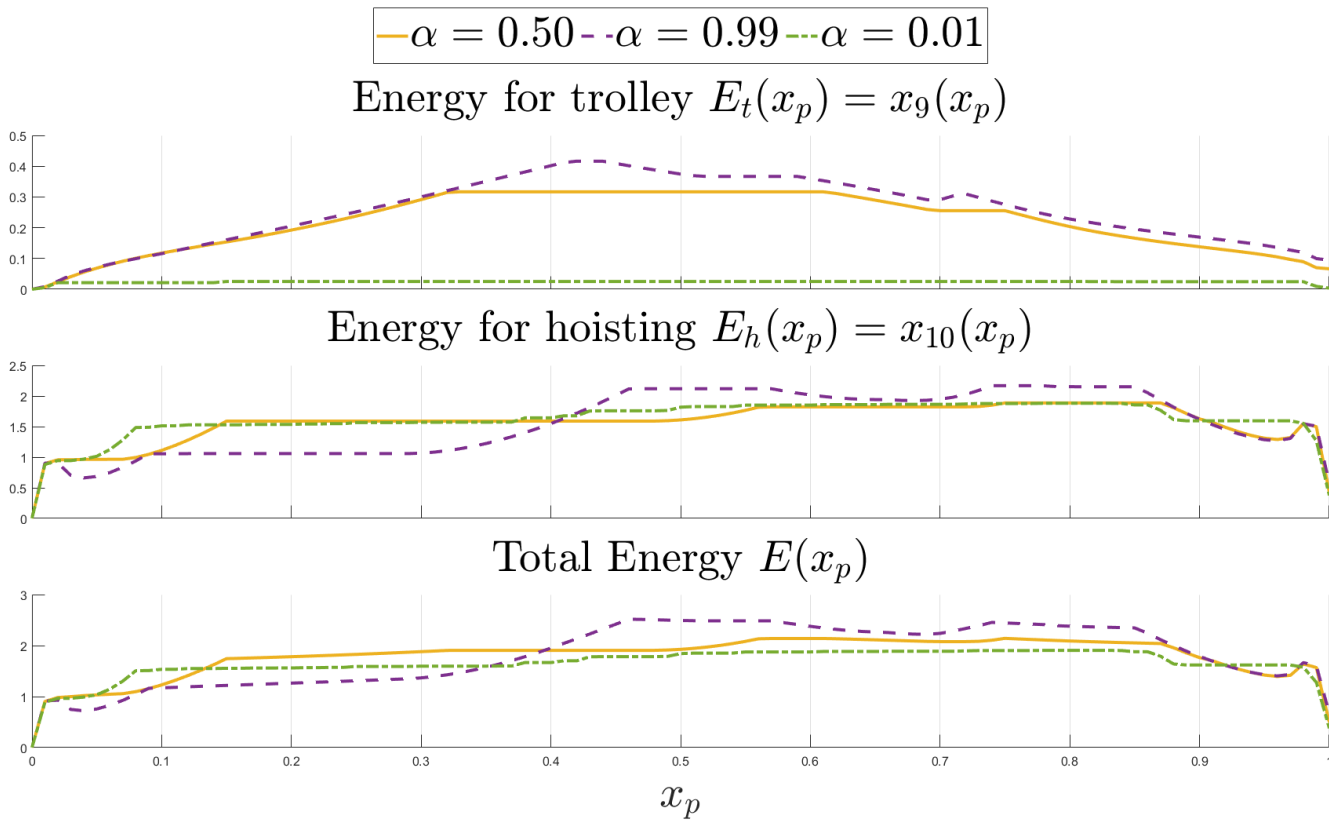
Example



Example



Example



About the reformulations

Advantages

- We no longer define an explicit function $s(x_p)$, but simply function values.
- Description of stack heights becomes trivial and easy to represent numerically.
- By standard epigraph reformulations, the model accounting for energy regeneration can be put in a form with improved numerical properties

About the reformulations

Limitations

- Payload moving monotonically in one direction which enforces no sway condition.
- Unifor discretization may lead to not capturing dynamics of the system in the beginning and the end.
- Dynamics and cost function remain non-convex and may lead to a solution at a local minimum.

About energy consumption

- The model for regeneration is still simple and a more complex one could be incorporated.
- By studying this small example, one note that there's room for energy reduction with minor increase in the loading time.

Summary

- **Objective:** Trade-off time and energy when loading a container ship.
- **Challenge:** Avoid collision with container stacks.
- **Idea:** Variable change in an optimal control problem and standard epigraph formulations.
- **Outcome:** Non-convex container avoidance constraints become linear bound constraints and energy consumption can be reduced with minor increase in loading time.

Thank you!